



DEPARTMENT OF PHYSICS

STIRLING HALL

Physics

Engineering Physics

Astronomy

Queen's University

Kingston, Canada

K7L 3N6

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Dear Alan :

Enclosed please find a few more notes. This discussion sets up a single algorithm for the construction of a multi-component jet. No iteration is required for the state variables, and the numerical work should present no problems (the eqns being only superficially complicated). Also enclosed is a little episode on Macsyma which reveals an error in previous notes.

Best wishes

Tayll

Streamline Relativistic Hydrodynamics of Jets

The problem:

If you assume that radio jets represent pressure confined outflows of matter, determine, under well defined but minimal assumptions, the confining pressure.

Solution:

First assume that the magnetic contribution to the confinement is negligible.

a) Background Hydrodynamics

Hydrodynamics is (given T^α_β)

$$\nabla_\alpha u^\alpha = 0, \quad (1)$$

with

$$\nabla_\alpha T^\alpha_\beta = 0. \quad (2)$$

Assume a perfect fluid,

$$T^\alpha_\beta = n h u^\alpha u_\beta + p \delta^\alpha_\beta, \quad (3)$$

where $h \equiv (\rho + p)/n$.

From (2)

$$(h u_n)^\circ + \Theta = 0. \quad (4)$$

With (1) through (4)

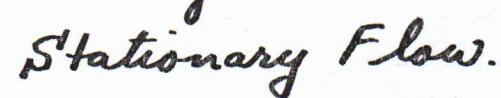
$$(h u_\beta)^\circ = -\frac{1}{n} \frac{\partial p}{\partial x^\beta} + \Gamma_{\beta\alpha}^\gamma h u^\alpha u_\gamma. \quad (5)$$

Ignore the gravitational field and use cylindrical coordinates [Minkowski space :

$$(r, \theta, \varphi, t) \text{ s.t. } \dot{t} = \gamma.$$

Assume that & scalar Φ

$$\frac{\partial \Phi}{\partial t} = \frac{\partial \Phi}{\partial \varphi} = 0. \quad (6)$$

 Cylindrical Symmetry.
 Stationary Flow.

With (6), (5) reads as

$$(h \gamma)^\circ = (h u_\varphi)^\circ = 0, \quad (7)$$

$$(h u_r)^\circ = \underline{u_\varphi^2} \frac{h}{r^3} - \frac{1}{n} \frac{\partial p}{\partial r}, \quad (8)$$

$$(h u_z)^\circ = -\frac{1}{n} \frac{\partial p}{\partial z}. \quad (9)$$

b) Restricted Velocity Field

We assume $\exists g = g(r) \ni$

$$\frac{\partial}{\partial r} \left(g(r) \frac{u^r}{u^\theta} \right) = 0. \quad (10)$$

Then (4) reads as

$$nr u^\theta = A g(r) \ni \dot{A} = 0. \quad (11)$$

c) Equation of Motion

From (7)

$$h \gamma = B, \quad \dot{B} = 0, \quad (12)$$

and

$$u_\theta = \gamma \bar{\Psi}, \quad \dot{\bar{\Psi}} = 0. \quad (13)$$

With (13),

$$\gamma^2 = \frac{r^2}{r^2 - \bar{\Psi}^2} \left\{ 1 + u^\theta \left(1 + \frac{u^r}{u^\theta} \right)^2 \right\}, \quad (14)$$

so that from the Bernoulli Eqn. (12)

$$\begin{aligned} u^\theta &= \frac{B^2 (r^2 - \bar{\Psi}^2) - h^2 r^2}{h^2 r^2 \left\{ 1 + u^r / u^\theta \right\}} \\ &= \frac{A^2 g^2(r)}{n^2 r^2} \end{aligned}$$

from (11) for a non-axial streamline. Thus

$$A^2 \left(\frac{h}{n} \right)^2 g^2(r) \left\{ 1 + \left(\frac{u^r}{u^\theta} \right)^2 \right\} = r^2 \left\{ B^2 (1 - \bar{\Psi}^2 / r^2) - h^2 \right\}. \quad (15)$$

d) Dimensionless Equation

Set $\Phi = 0$ ($\dot{\varphi} = 0$) here. Consider a fiducial point \hat{o} along the streamline. Define

$$r/r_0 \equiv y$$

$$z/r_0 \equiv x + z_0/r_0$$

$$h/n_0 \equiv N(x)$$

$$h/h_0 \equiv H(x)$$

$$g/g_0 \equiv G = G(y, r_0)$$

$$1 + \left(\frac{dy}{dx}\right)_0^2 \equiv \alpha$$

} The streamline defines $y(x)$,
 N & H are streamline functions.

Then, (15) reduces to

$$\left(\frac{dy}{dx}\right)^2 - f y^2 + 1 = 0 \quad (16)$$

$$\Rightarrow f = \left(\frac{N}{H}\right)^2 \alpha \frac{(y_0^2 - H^2)}{G^2 (y_0^2 - 1)}. \quad (17)$$

Clearly $f > 0$ for real solutions y . Solutions to (16) are not unique : e.g. if $f = \beta = \text{const.}$

$$y = 1/\sqrt{\beta} \quad \& \quad y = \frac{1}{\sqrt{\beta}} \cosh \sqrt{\beta} x.$$

why? — The Euler Eqns. (8) & (9)
 have not been used!

\Rightarrow Invert (16) & (17) :

$$\frac{1}{\alpha} \left(\frac{G}{y}\right)^2 / \left(\left(\frac{dy}{dx}\right)^2 + 1\right) = \left(\frac{N}{H}\right)^2 \frac{(y_0^2 - H^2)}{(y_0^2 - 1)}, \quad (18)$$

take $y(x)$ as given (observed).

This demands that the observed y can be taken as a streamline.

e) Equation of State

We suppose that the gas is
an ideal neutral mix of protons & electrons.

i) $N:$
$$N = \sqrt{\frac{L(\chi_e^0)}{L(\chi_e)} \frac{L(\chi_p^0)}{L(\chi_p)}}$$

 $\Rightarrow L \equiv \frac{\chi}{K_2(\chi)} \exp \left\{ -\chi \frac{K_3(\chi)}{K_2(\chi)} \right\}, \chi = \frac{mc^2}{kT}$
 $L \sim \begin{cases} \sqrt{\frac{2}{\pi}} \chi^{3/2}, & \chi \gg 1 \text{ (Cold)} \\ \frac{1}{2} \chi^3 e^{-4}, & \chi \ll 1 \text{ (Hot)} \end{cases}$
 $\therefore N \sim \begin{cases} (T/T_0)^{3/2}; kT \ll m_e c^2 & ^+ \\ (T/T_0)^{9/4}; m_e c^2 \ll kT \ll m_p c^2 & ^+ \end{cases}$
 $+ T \ll 6 \cdot 10^9 K, \quad ^+ 6 \cdot 10^9 K \ll T \ll 10^{13} K.$

ii) $\hbar:$
$$\hbar = \frac{\sum_i n_i m_i G(\chi_i)}{\sum_j n_j}$$

 $m = mc^2 \Rightarrow G(\chi) \equiv \frac{K_3(\chi)}{K_2(\chi)} \sim \begin{cases} 1 + 5/2 \chi, & \chi \gg 1 \text{ (Cold)} \\ 4/\chi, & \chi \ll 1 \text{ (Hot)} \end{cases}$
 $\therefore \hbar \sim \begin{cases} \frac{m_e + m_p}{2} \sim \frac{m_p}{2}; kT \ll m_e c^2 \\ 2kT + \frac{m_p}{2} \sim \frac{m_p}{2}; m_e c^2 \ll kT \ll m_p c^2 \end{cases}$

$$\therefore H \sim 1$$

$$\therefore \frac{\gamma_0^2 - H^2}{\gamma_0^2 - 1} \sim 1$$

iii) $p:$
$$p = \sum_i n_i kT$$

 $\Rightarrow P = N \left(\frac{T}{T_0} \right) \Rightarrow P = \frac{p}{p_0}$

$$\therefore \left(\frac{N}{H}\right)^2 \left(\frac{\gamma_0^2 - H^2}{\gamma_0^2 - 1}\right) \approx \begin{cases} \rho^{6/5} & ; kT \ll m_e c^2 \\ \rho^{18/13} & ; m_e c^2 \ll kT \ll m_p c^2 \end{cases} \quad (19)$$

From (18) & (19) then

$$\frac{1}{\alpha} \left(\frac{G}{y}\right)^2 \left(\left(\frac{dy}{dx}\right)^2 + 1\right) \approx \begin{cases} \rho^{6/5} & ; kT \ll m_e c^2 \\ \rho^{18/13} & ; m_e c^2 \ll kT \ll m_p c^2 \end{cases} \quad (20)$$

From (12)

$$H\gamma = \gamma_0 \quad (21)$$

so that $\gamma \approx \text{const.}$ for $H \approx 1$.

f) ρ The analysis is restricted to a streamline "boundary". The boundary ought to be a boundary surface:

$$(T_\beta^\alpha n_\alpha n^\beta)^- = (T_\beta^\alpha n_\alpha n^\beta)^+ \quad (22)$$

whereas $T_\beta^\alpha^- = nh u^\alpha n_\beta + p \delta_\beta^\alpha$,

write $T_\beta^\alpha^+ = \bar{n} \bar{h} U^\alpha U_\beta + \bar{p} \delta_\beta^\alpha$

$$\Rightarrow U^\alpha = (0, 0, 0, 1) \quad (\text{Static cloud}).$$

$$\text{Then (22)} \Rightarrow p = \bar{p} + \bar{n} \bar{h} (U^\alpha n_\alpha)^2.$$

$$\text{But } U^\alpha n_\alpha = n_t = 0 \quad (\text{Static flow})$$

$$\therefore p = \bar{p},$$

i.e. ρ gives the dimensionless pressure of the external cloud (i.e. in the rest frame of the cloud).

g) Procedure From (20) then
assumed velocity field

$$\rho = \left\{ \frac{1}{a} \left(\frac{G}{y} \right)^2 \left(\left(\frac{dy}{dx} \right)^2 + 1 \right) \right\}^{\delta} \Rightarrow \delta = \begin{cases} 5/6 & ; kT \ll m_ec^2 \\ 13/18 & ; m_ec^2 \ll kT \end{cases}$$

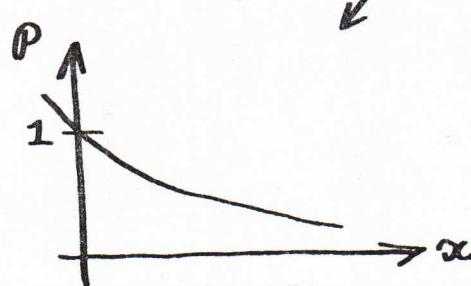
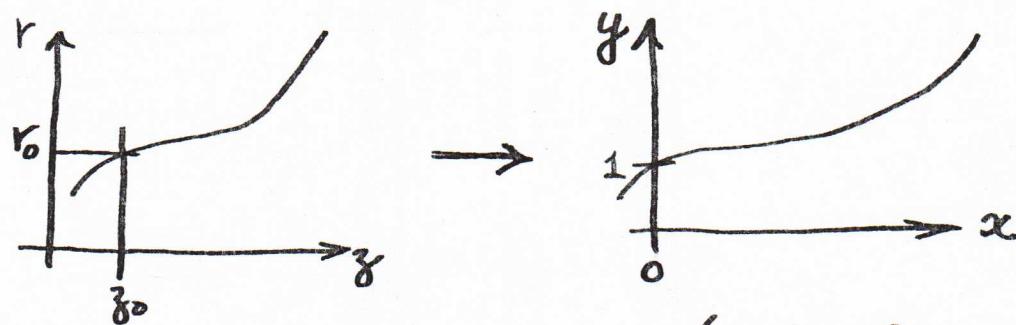
~~DEGBMATH~~

\uparrow
 external
 Cloud.
 \uparrow
observed

The "parameter space" is simply G.

Need α, r_0, y_0 .

Take an observed part of the jet as
 the fiducial point.



with G



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Dear Alan:

Nov 12/80

If what I enclose is correct, Dick's streamline approach (when corrected) and my approach finally give the same equations. The extra term indicates that a thermal component will change d^2R/dz^2 in, perhaps, an important way, and hence the shape of the boundary $R(z)$. As the 'bulk' energy becomes relativistic, the term probably does not contribute much. However, a thermal component will change even a 'fast' jet.

Kayll

Refer to the notes : Relativistic non-Magnetic Steady Jets (A) :

- p.5 : The continuity eqn. actually reads $\{R^2 w_3 n\}^* = 0$ so $n \neq n(z)$ in general.
- p.8 : From the $w_r dw_r/dz|_B$ & $w_z dw_z/dz|_B$ eqns. of the Summary we have:

$$(*) \quad \omega_z^2 \frac{d^2 R}{dz^2} = \frac{\gamma_B^2 \psi_s^2}{R^3} + \frac{\alpha}{\delta_B R} (\rho_i - \rho_E) \left(1 + \left(\frac{dR}{dz}\right)^2\right) + \frac{1}{\delta_B} \left(\frac{dR}{dz}\right) \frac{dp_E}{dz}.$$

New Summary for u-similarity :

Continuity : $\{R^2 w_3 n\}^* = 0$ so $R^2 w_3 n = f(r/R)$

Bernoulli : $\{\xi \gamma\}^* = 0$ so $\xi \gamma = \delta \gamma/n = g(r/R)$

Boundary : $dR/dz = w_r/w_z$

Rotation : $w_\varphi = \gamma \psi/R \Rightarrow \psi^* = 0 \quad (\psi_B = \psi_s)$

Euler : (*) given above.

Here $* \equiv u_r \partial/\partial r + u_z \partial/\partial z$, $\gamma_B^2 = 1 + w^2/c^2$ ($\approx 1 + w_z^2/c^2$), and $\delta_B = \rho_i + \rho_E = \rho_B + \rho_B$ (in appropriate units, see below).

Compare Dick's Eqs. (Oct 30/80 p. 14). i) $n h (\equiv \delta)$ is $n h|_B$. ii) To get his (*), linearize (drop $(dR/dz)^2$ and dp_E/dz terms) (*) here.

Questions : i) Is it in fact much more difficult to solve (numerically) the unlinearized form (*)?

- ii) Are there no cases when the $d\rho_e/dz$ term will be of interest? (It may be that we can make some interesting jets with this term included.)
- iii) Use $dR/dz = w_r/w_z$ and $w_\varphi = \gamma \psi/R$ in the exact form for δ_B^2 to re-write (*) in the form:

$$(*)' \quad \frac{w_z^2 d^2 R}{dz^2} = \frac{\psi_s^2 c^2}{R(c^2 R_s^2 - \psi_s^2)} + \frac{1}{R} \left(1 + \left(\frac{dR}{dz} \right)^2 \right) \left(\frac{2(p_j - \rho_e)}{\delta_B} + \frac{\psi_s^2 w_z^2}{c^2 R_s^2 - \psi_s^2} \right) + \frac{1}{\delta_B} \left(\frac{dR}{dz} \right) \frac{dp_e}{dz}$$

Though $\delta_B^2 \approx 1 + w_z^2/c^2$ can be an excellent approximation, is it in fact more difficult to handle (numerically) the above exact eqn.? If $c^2 R_s^2 > \psi_s^2$ then, with accuracy guaranteed we can use ψ_s^2/R^3 for the first term and $(\psi_s/R)^2 (w_z/c)^2$ for the second term in the second bracket. The "relativistic" terms are then just the $(w_z/c)^2$ term and the form of δ_B , in (*').

Change
units of A
why?

Units: We use std. (but relativistic) units. Take $[p] = [\delta]$ (see below) so replace δ above by δ/c^2 in these eqns. i.e. $[\psi] = L^2/t$, $[(*)'] = [(*)] = L/t^2$, with the $/c^2$ added to δ and $[p]$ taken = $[\delta]$.

→ Eqn. of State: Take the std. relativistic Maxwell-Boltzmann gas, and choose T as the "fundamental" variable (i.e. n, p, ρ as fns of T)

$\eta \equiv \# \text{ baryons/unit vol. in local rest frame}; \rho \stackrel{?}{=} T^{\alpha\beta} u_\alpha u_\beta$

$$\rho \stackrel{?}{=} T^{\alpha\beta} n_\alpha n_\beta = \frac{1}{3} T^{\alpha\beta} (u_\alpha u_\beta + \eta_{\alpha\beta})$$

$$[p] = [p] \quad p = n k T,$$

$$M L^{-1} t^{-2}. \quad \rho = p(3 + \chi k_1(x)/k_2(x)) \quad \exists \quad \chi \equiv mc^2/kT,$$

single comp. free gas case.

(3)

$$\therefore \delta = p + \rho = \rho(4 + \chi K_1 / K_2), \quad [\delta] = [\rho].$$

[n]
L⁻³

$$n = \frac{L}{k} T K_2 \exp(\chi K_1 / K_2) \quad \Rightarrow \quad L = \exp(4 - \delta/k) \cdot 4\pi m^2 c k / h^3$$

δ = specific entropy (const. here as in all perf. fluids.)

(Note: $[\rho^2 \omega_z n] = t^{-1}$, $[\delta \propto / n c^2] = M.$)

$$\left. \begin{aligned} \therefore p &= (L/k) T^2 K_2 \exp(\chi K_1 / K_2) \\ \delta &= (L/k) T^2 (4K_2 + \chi K_1) \exp(\chi K_1 / K_2) \\ \delta/n &= kT(4 + \chi K_1 / K_2) \\ m &= \text{const.}, \quad T = T(z), \quad K_n = K_n(\chi), \quad \chi \equiv mc^2 / kT. \end{aligned} \right\} \begin{matrix} \text{single comp.} \\ \text{eqn. of state} \end{matrix}$$

Continuity Eqn. reads:

$$\left(\frac{\rho}{\rho_s} \right)^2 \left(\frac{\omega_z}{\omega_{z_s}} \right) \left(\frac{T}{T_s} \right) \left(\frac{K_2}{K_{2s}} \right) \exp(\chi K_1 / K_2 - \chi_s K_{1s} / K_{2s}) = 1.$$

Bernoulli Eqn. reads:

$$\begin{aligned} \left(\frac{\delta}{\delta_s} \right)_B \left(\frac{T}{T_s} \right) \left(\frac{4 + \chi K_1 / K_2}{4 + \chi_s K_{1s} / K_{2s}} \right) &= 1, \\ \Rightarrow \left(\frac{\delta}{\delta_s} \right)_B &= \left(\frac{\rho}{\rho_s} \right) \left(\frac{\rho_s^2 c^2 - \psi_s^2}{\rho^2 c^2 - \psi^2} \cdot \frac{1 + (\omega_z/c)^2 (1 + (dR/dz)^2)}{1 + (\omega_{z_s}/c)^2 (1 + (dR/dz_s)^2)} \right)^{1/2} \\ &= \left(\frac{1 + (\omega_z/c)^2 (1 + (dR/dz)^2)}{1 + (\omega_{z_s}/c)^2 (1 + (dR/dz_s)^2)} \right)^{1/2} \quad \text{for } \rho_s^2 c^2 \gg \psi_s^2. \end{aligned}$$

For the Euler Eqn.:

Pressure gradient

$$\frac{C^2}{\delta_B} \left(\frac{dR}{dz} \right) \frac{dp}{dz} = \frac{C^2}{4 + \chi K_1 / K_2} \left(\frac{dR}{dz} \right) \frac{d \ln p}{dz},$$

$$\frac{d \ln p}{dz} = \frac{1}{T} \frac{dT}{dz} \left\{ 4 - \chi \left(\frac{3K_1}{K_2} + \chi \left(\left(\frac{K_1}{K_2} \right)^2 - 1 \right) \right) \right\}.$$

$$-\frac{C^2 p \bar{e}}{\delta_B} = -\frac{C^2 K_2}{4K_2 + \chi K_1} = -\frac{C^2}{4 + \chi K_1 / K_2}$$

To complete Euler Eqn. need p_i . Apply Bernoulli along axis

$$\left(\frac{1 + (\omega_{zS}/c)^2}{1 + (\omega_z/c)^2} \right) \left[\left(\frac{T}{T_S} \right) \left(\frac{4 + \chi K_1 / K_2}{4 + \chi_S K_{1S} / K_{2S}} \right) \right]_S = 1$$

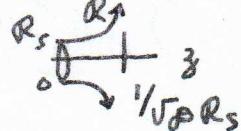
Aside: Suppose $T = T_S$ (isothermal cloud). From continuity $(R/R_S)^2 = \omega_{zS}/\omega_z$. From Bernoulli $(\gamma/\gamma_S)_B = 1$ so if $R_S^2 c^2 \gg \psi_S^2$

$$\begin{aligned} 1 + (dR/dz)^2 &= (\omega_{zS}/\omega_z)^2 (1 + (dR/dz)_S^2) \\ &= \frac{R^4}{R_S^4} (1 + (dR/dz)_S^2) \end{aligned}$$

$$\therefore 1 + (dR/dz)^2 = DR^4, D \text{ const.}$$

$$\therefore \int_s^y \frac{dR}{\sqrt{DR^4 - 1}} = y, DR^4 \gg 1 \approx R = R_S (1 - 3\sqrt{\rho} R_S)$$

From Euler ($\partial \psi_S = 0$)



$$\omega_z^2 d^2 R / dz^2 = \epsilon R^3 (p_S - p \bar{e}), \epsilon \text{ const}$$

$$\text{so } d^2 R / dz^2 = \epsilon R^7 (p_S - p \bar{e}). \text{ But with Bernoulli } \& DR^4 \gg 1, d^2 R / dz^2 = g R \text{ so } (p_S - p \bar{e}) \propto 1/R^6.$$

Ultra-Relativistic Energies : $kT \gg mc^2$

$$K_2 \sim 2/\chi^2 \sim 2\hbar^2 T^2 / m^2 c^4 \quad \left. \right\} \chi K_1 / K_2 \sim 0$$

$$K_1 \sim 1/\chi \sim \hbar T / mc^2 \quad \left. \right\} \chi (3K_1 / K_2 + \chi ((K_1 / K_2)^2 - 1)) \sim 0$$

$$\text{Continuity} \rightarrow \left(\frac{R}{R_S} \right)^2 \left(\frac{\omega_z}{\omega_{zS}} \right) \left(\frac{T}{T_S} \right)^3 = 1$$

$$\text{Bernoulli} \rightarrow \left(\frac{\gamma}{\gamma_S} \right)_B \left(\frac{T}{T_S} \right) = 1$$

(5)

$$\frac{c^2}{\delta_B} \left(\frac{dR}{dz} \right) \frac{dp_E}{dz} \sim \frac{c^2}{T} \frac{dT}{dz} \frac{dR}{dz}, \quad -\frac{c^2 p_E}{\delta_B} \sim -\frac{c^2}{4},$$

axis $\rightarrow \frac{1 + (\omega_z/c)^2}{1 + (\omega_{zs}/c)^2} \left(\frac{T_s}{T_{ss}} \right) = 1.$

Classical Energies: $kT \ll mc^2$

$$K_1 \sim K_2 \sim \sqrt{\frac{\pi}{2x}} e^{-x}, \quad x K_1 / K_2 \sim x$$

$$x(3K_1/K_2 + x(K_1^2/K_2^2 - 1)) \sim 3x.$$

Continuity $\rightarrow \left(\frac{R}{R_s} \right)^2 \left(\frac{\omega_z}{\omega_{zs}} \right) \left(\frac{T}{T_s} \right)^{3/2} = 1$

Bernoulli $\rightarrow \left(\frac{\gamma}{\gamma_s} \right)_B \left(\frac{4kT + mc^2}{4kT_s + mc^2} \right) = 1 \simeq \left(\frac{\gamma}{\gamma_s} \right)_B.$

$$\begin{aligned} \frac{c^2}{\delta_B} \left(\frac{dR}{dz} \right) \frac{dp_E}{dz} &\rightarrow \frac{c^2}{4kT + mc^2} \left(\frac{dR}{dz} \right) \frac{1}{T} \frac{dT}{dz} \left\{ 4kT - 3mc^2 \right\} \\ &\simeq -\frac{3c^2}{T} \frac{dT}{dz} \left(\frac{dR}{dz} \right) \end{aligned}$$

$$-\frac{c^2 p_E}{\delta_B} \rightarrow -\frac{c^2 kT}{4kT + mc^2} \simeq -\frac{kT}{m},$$

axis $\rightarrow \left(\frac{1 + (\omega_z/c)^2}{1 + (\omega_{zs}/c)^2} \right) \left[\frac{4kT + mc^2}{4kT_s + mc^2} \right]_s = 1 \simeq \frac{1 + (\omega_z/c)^2}{1 + (\omega_{zs}/c)^2}$

$$2b_s c^2 / \delta_B \rightarrow \frac{2k c^2 T_s^{5/2}}{T^{3/2} (4kT + mc^2)} \simeq \frac{2k T_s^{5/2}}{m T^{3/2}}$$

[Classical theory has low energy & low vel. so

$$\omega_z^2 \frac{d^2 R}{dz^2} = \frac{\psi_s^2}{R^3} + \frac{1}{R} \left(1 + \left(\frac{dR}{dz} \right)^2 \right) \left(\frac{2k}{m T^{3/2}} \right) \left(T_s^{5/2} - T^{5/2} \right) - \frac{3c^2}{T} \frac{dT}{dz} \frac{dR}{dz}.$$

Multi-component gas: (i species)

Specify m_i , T_i

then $\rho = \sum_i \rho_i$, $\rho = \sum_i \rho_i$, $N = \sum_i N_i$, $\delta = \sum_i \delta_i$.

Can proceed as with $i=1$ (single component) but sum
for a thermal (γ) and relativistic (\hat{R}) 2-component
model, specify m_T & m_R (fixed). One
additional free function must be specified, e.g.
 $T_T / T_R \equiv \tilde{T} (= T(r/R) \text{ if } \alpha^* = 0)$.

Arno's Procedure

- ① Specify an equation of state along the jet axis (j). Use Bernoulli along the axis so

$$\frac{\gamma}{\gamma_s} \Big|_s = \frac{n}{n_s} \frac{\gamma_s}{\gamma} \Big|_j$$

$$\Rightarrow w_z(z) / w_z^s.$$

- ② Use Continuity along the boundary (B)

$$\frac{R}{R_s} = \sqrt{\frac{n_s}{n_B} \frac{w_z^s}{w_z(z)}}$$

If we know n_B then R is known. But n_B must be $n_B(z)$, which in turn must be n_j , which we have specified in ①.

Thus R is already known.

Further Notes

first we
clarified
eqns?

Though $p = p(z)$ along a streamline, across the jet $p \neq p(z)$, it is governed by the homology. But $p = n k T$ (e.g. 1 component) & $n = n(z)$, $\therefore T \neq T(z)$ across the jet, T is also governed by the homology. Thus the jet is already 2-dimensional in T , and with $\rho_s > \rho_B$, $T_B < T_s$. This is extended to a mixture as in notes (E), for this procedure apply (E) along the axis (ideal gas, $T \neq 0$)

We still need Euler: Suppose $\Psi = 0$ (no rotation), then

$$\omega_z^2 \frac{dR}{dz^2} = \frac{2c^2(\rho_s - \rho_B)(1 + (dR/dz)^2)}{\delta_B R} + \frac{c^2}{\delta_B} \left(\frac{dR}{dz} \right) \frac{dp_E}{dz}$$

algebraic (Since we know R , we find δ_B from Bernoulli along B .)

Euler now gives p_E . The jet constructed needs a background, and Euler gives the required one.

$$p_E \approx -\delta_B R \omega_z^2 d^2 R / dz^2 / 2c^2(1 + (dR/dz)^2) + p_s$$

Given the jet (axial construction as above) & given a background, you must adjust Ψ for a consistent Euler eqn. (Euler is now at worst 1st order)

- ρ_s is, in general $\neq \rho_B$ as written previous in notes

- drop (3) & following in (B).
homologous

Relativistic jets :

- non-magnetic, non-rotating - { one comp.; mix. }
- magnetic, "
- not ?

Relativistic Non-Magnetic Steady Jets

Notation: $T^{\alpha\beta} = (\rho + p/c^2) u^\alpha u^\beta + p \gamma^{\alpha\beta}$
 $u^\alpha = \gamma(1, v^i)$; $\gamma = 1/\sqrt{1 - v^2/c^2}$; $u^\alpha u_\alpha = -1$.

Euler Eqn: $\nabla \left(\frac{v^2}{2}\right) + \frac{1}{\gamma^2(\rho + p/c^2)} \nabla p = \tilde{v} \times (\nabla \times \tilde{v})$ (1)

Continuity: $\gamma \tilde{v} \cdot \nabla p + (\rho + p/c^2) \nabla \gamma \tilde{v} = 0$ (2)

(The Bernoulli Eqn. $\tilde{v} \cdot \mathbf{0} = 0$ not used here.)

Assume axial symmetry (no of dept. terms), $\mathbf{*} = v_r \frac{\partial}{\partial r} + v_\theta \frac{\partial}{\partial \theta}$
 then the components of $\mathbf{0}$ read

$$v_r^* = \frac{v_\theta^2}{r} - \frac{1}{\gamma^2(\rho + p/c^2)} \frac{\partial p}{\partial r}, \quad (1a)$$

$$v_\theta^* = -\frac{v_r v_\theta}{r} \Rightarrow v_\theta^* = \frac{L}{r} \Rightarrow L^* = 0, \quad (1b)$$

$$v_\theta^* = -\frac{1}{\gamma^2(\rho + p/c^2)} \frac{\partial p}{\partial \theta}. \quad (1c)$$

Continuity reads

$$\gamma^* p = -(\rho + p/c^2) \left\{ \gamma^* + \gamma \left(\frac{\partial v_r}{\partial r} + \frac{\partial v_\theta}{\partial r} + \frac{\partial v_\theta}{\partial \theta} \right) \right\}. \quad (2a)$$

Similarity Forms:

$$p = p_s - (\rho_s - \rho_R) \left(\frac{r}{R} \right)^2$$

$$L = \Omega R_A^2 \left(\frac{r}{R} \right)^2$$

$$\tilde{v} = \left(\omega_r \left(\frac{r}{R} \right), \omega_\theta \left(\frac{r}{R} \right), \omega_\theta \right)$$

along the boundary streamline then

$$\frac{dR}{dz} = \frac{\omega_r}{\omega_z},$$

$$\omega_z \frac{d\omega_r}{dz} = \frac{\Omega^2 R_A^4}{R^3} + \frac{2(p_s - p_R)}{\gamma_R^2 (\rho + p_R/c^2) R}, \quad (1a')$$

$$\omega_\varphi = \frac{\Omega R_A^2}{R}$$

$$\omega_z \frac{d\omega_z}{dz} = -\frac{1}{\gamma_R^2 (\rho + p_R/c^2)} \left\{ \frac{dp_R}{dz} + 2 \frac{\omega_r}{\omega_z} \cdot \frac{(p_s - p_R)}{R} \right\}, \quad (1c')$$

$$\omega_z \frac{dp}{dz} = -(\rho + p_R/c^2) \left\{ \frac{2\omega_r}{R} + \frac{d\omega_z}{dz} + \frac{\gamma_R^2 \omega_z}{2c^2} \frac{d\omega^2}{dz} \right\}, \quad (2a')$$

where $p_R(z)$ given

$$\omega^2 = \omega_r^2 + \omega_\varphi^2 + \omega_z^2$$

$$\gamma_R = 1/\sqrt{1 - \omega^2/c^2}.$$

-
- Specify equation of state,
 - to get non-relativistic case set all terms $\frac{c^2}{c^2} = 0$.

(3)

Components of the Euler eqn. ⑤ read

$$\left. \begin{aligned} \omega_r \frac{d\omega_r}{dz} &= \frac{dR}{dz} \left\{ \frac{\psi^2}{R^3} - \left(\frac{R}{r}\right) \frac{1}{\gamma^2 \delta} \frac{\partial p}{\partial r} \right\} \\ \omega_\theta &= \frac{\psi}{R} \Rightarrow \psi^* = 0 \\ \omega_z \frac{d\omega_z}{dz} &= - \frac{1}{\gamma^2 \delta} \frac{\partial p}{\partial z} \end{aligned} \right\} \quad (7)$$

For the continuity eqn. ③ $\gamma \rho^* + \delta \dot{\gamma}^* + \delta \gamma \vec{v} \cdot \vec{v} = 0$

$$\vec{v} \cdot \vec{v} = \frac{2\omega_r}{R} + \frac{d\omega_z}{dz} = \omega_z \frac{d \ln R^2 \omega_z}{dz}$$

$$\dot{\rho}^* = \omega_r \left(\frac{r}{R}\right) \frac{\partial p}{\partial r} + \omega_z \frac{\partial p}{\partial z} = \omega_z \frac{dp}{dz} \quad \text{for } \underline{p = p(z)}$$

$$\dot{\gamma}^* = \frac{\gamma^3}{2c^2} \left\{ \left(\frac{r}{R}\right)^2 \left(\dot{\omega}_r^2 + \dot{\omega}_\theta^2 \right) + \dot{\omega}_z^2 \right\}$$

$$\dot{\omega}_r^2 = 2\omega_r \omega_z \frac{d\omega_r}{dz} = 2\omega_z \frac{dR}{dz} \left\{ \frac{\psi^2}{R^3} - \left(\frac{R}{r}\right) \frac{1}{\gamma^2 \delta} \frac{\partial p}{\partial r} \right\}$$

$$\dot{\omega}_\theta^2 = -2\omega_\theta^2 \omega_r = -2 \frac{\psi^2}{R^3} \omega_z \frac{dR}{dz}$$

$$\dot{\omega}_z^2 = 2\omega_z^2 \frac{d\omega_z}{dz} = -2 \frac{\omega_z}{\gamma^2 \delta} \frac{\partial p}{\partial z}$$

$$\therefore \dot{\gamma}^* = -\frac{\gamma \omega_z}{c^2 \delta} \left\{ \left(\frac{r}{R}\right) \frac{\partial p}{\partial r} \frac{dR}{dz} + \frac{\partial p}{\partial z} \right\}$$

Thus the continuity eqn. reads

$$\delta \frac{d \ln R^2 \omega_z}{dz} + \frac{\partial p}{\partial z} + \left(\frac{r}{R}\right) \frac{\partial p}{\partial r} \frac{dR}{dz} - \frac{1}{c^2} \left\{ \left(\frac{r}{R}\right) \frac{\partial p}{\partial r} \frac{dR}{dz} + \frac{\partial p}{\partial z} \right\} = 0 \quad (8)$$

Again let $p = p_s - (p_s - p_E) \left(\frac{r}{R}\right)^2 \Rightarrow p = p(z)$ ⑨⁽⁴⁾

$$\therefore \begin{cases} \frac{\partial p}{\partial r} = \frac{2r}{R^2} (p_E - p_s) \\ \frac{\partial p}{\partial z} = \frac{dp_s}{dz} + \left(\frac{r}{R}\right)^2 \left(\frac{dp_E}{dz} - \frac{dp_s}{dz}\right) - \frac{2}{R} \left(\frac{r}{R}\right)^2 \frac{dR}{dz} (p_E - p_s) \end{cases}$$

$$\Rightarrow \left(\frac{r}{R}\right) \frac{\partial p}{\partial r} \frac{dR}{dz} + \frac{\partial p}{\partial z} = \frac{dp_s}{dz} + \left(\frac{r}{R}\right)^2 \left(\frac{dp_E}{dz} - \frac{dp_s}{dz}\right)$$

Summary: Under the v-similarity & ⑨ & $p = p(z)$:

$$\frac{dR}{dz} = \frac{\omega_r}{\omega_z}$$

$$\gamma_B = 1/\sqrt{1-\omega^2/c^2} \quad \omega_g = \frac{\psi}{R}, \quad \psi^* = 0 \quad (\omega_g \neq \omega_g(z))$$

$$\delta_B = p_s + p_E/c^2$$

$$\omega_r \frac{d\omega_r}{dz} \Big|_B = \frac{dR}{dz} \left\{ \frac{\psi^2}{R^3} + \frac{2(p_s - p_E)}{R \gamma_B^2 \delta_B} \right\}$$

$$\delta_s = p_s + p_s/c^2$$

$$\omega_z \frac{d\omega_z}{dz} \Big|_B = -\frac{1}{\gamma_B^2 \delta_B} \left\{ \frac{dp_E}{dz} + \frac{2}{R} \frac{dR}{dz} (p_s - p_E) \right\}$$

Continuity

$$\delta_j \frac{d \ln R^2 \omega_z}{dz} + \frac{dp}{dz} - \frac{1}{c^2} \left\{ \frac{dp_s}{dz} + \left(\frac{r}{R}\right)^2 \left(\frac{dp_E}{dz} - \frac{dp_s}{dz}\right) \right\} = 0$$

$$\text{on axis: } \delta_j \frac{d \ln R^2 \omega_z}{dz} + \frac{dp}{dz} - \frac{1}{c^2} \frac{dp_s}{dz} = 0$$

$$\text{on boundary: } \delta_B \frac{d \ln R^2 \omega_z}{dz} + \frac{dp}{dz} - \frac{1}{c^2} \frac{dp_E}{dz} = 0$$

$$\therefore \left(\frac{p_s - p_E}{c^2} \right) d \frac{\ln R^2 \omega_3}{dz} = \frac{d}{dz} \left(\frac{p_s - p_E}{c^2} \right)$$

$$\therefore \frac{p_s - p_E}{c^2} \propto R^2 \omega_3 \quad (10)$$

(10) is a relativistic result for v -similarity.

Classical result: drop $\frac{1}{c^2}$ terms so $R^2 \omega_3 \rho = \text{const.}$

$$4: \underline{v\text{-similarity}}: u_r = \omega_r \left(\frac{r}{R} \right), u_\varphi = \omega_\varphi \left(\frac{r}{R} \right), u_z = \omega_3.$$

Continuity: from ① $\nabla \cdot n \underline{u} = n \nabla \cdot \underline{u} + \underline{u} \cdot \nabla n = 0; \underline{u} \equiv \gamma \underline{v}$

$$\therefore n \left\{ \frac{u_r}{r} + \frac{\partial u_r}{\partial r} + \frac{\partial u_3}{\partial z} \right\} + u_r \frac{\partial n}{\partial r} + u_3 \frac{\partial n}{\partial z} = 0.$$

$$\therefore n \left\{ 2 \frac{\omega_r}{R} + \frac{d \omega_3}{d z} \right\} + \omega_3 \frac{dn}{dz} = 0 \quad \underline{\omega_{r,z} = \omega(z), n = n(z)}$$

$$\therefore n \omega_3 d \frac{\ln R^2 \omega_3}{dz} + \omega_3 \frac{dn}{dz} = 0 \Rightarrow \boxed{R^2 \omega_3 n = \text{const.}} \quad (11)$$

Euler: Since $(\nabla \gamma)^* = 0$ from p.② we have

$$(\nabla u_r)^* = \frac{\nabla \gamma v_\varphi^2}{r} - \frac{\nabla}{\gamma r} \frac{\partial p}{\partial r} = \frac{\nabla}{\gamma} \left(\frac{u_\varphi^2}{r} - \frac{1}{r} \frac{\partial p}{\partial r} \right) \quad \left. \right\}$$

$$(\nabla u_\varphi)^* = - \frac{\nabla \gamma v_r v_\varphi}{r} = - \frac{\nabla u_r u_\varphi}{\gamma r} \quad \left. \right\}$$

$$(\nabla u_z)^* = - \frac{\nabla}{\gamma r} \frac{\partial p}{\partial z} \quad \left. \right\}$$

$$\therefore \frac{r}{\gamma} \omega_r \frac{d\omega_r}{dz} + \omega_r \gamma \frac{dR}{dz} (\ln \xi)^* = \frac{dR}{dz} \left\{ \frac{\omega_g^2}{R} - \frac{R}{r} \frac{1}{\gamma} \frac{\partial p}{\partial r} \right\}$$

$$\stackrel{*}{=} \omega_z \frac{d\omega_z}{dz} + \omega_z \gamma (\ln \xi)^* = -\frac{1}{\gamma} \frac{\partial p}{\partial z}$$

$$\stackrel{*}{=} v_\varphi = \frac{\mathcal{L}}{r} \Rightarrow \stackrel{*}{\mathcal{L}} = 0.$$

$$\frac{\omega_g^2}{R} = \frac{\gamma^2 \psi^2}{R^3} \leftarrow \omega_g = \gamma \left(\frac{R}{r} \right) v_\varphi = \frac{\gamma R \mathcal{L}}{r^2} = \frac{\gamma \mathcal{L}}{R} \left(\frac{R}{r} \right)^2 = \frac{\gamma \psi}{R} \Rightarrow \stackrel{*}{\psi} =$$

$$\therefore \stackrel{*}{\omega_g} = \frac{\psi \stackrel{*}{\gamma}}{R} - \frac{\psi \gamma \stackrel{*}{R}}{R^2} = \frac{\psi}{R} \left(\stackrel{*}{\gamma} - \frac{\omega_r}{R} \right)$$

from Bernoulli Eqn $(\ln \xi)^* = -(\ln \gamma)^*$

$$(\ln \gamma)^* = \frac{\stackrel{*}{\gamma}}{\gamma} = \frac{1}{2\gamma^2} \left\{ 1 + \frac{1}{c^2} \left(\left(\frac{r}{R} \right)^2 (\omega_r^2 + \omega_g^2) + \omega_z^2 \right) \right\}^*$$

$$= \frac{1}{2c^2 \gamma^2} \left\{ \left(\frac{r}{R} \right)^2 (\stackrel{*}{\omega}_r^2 + \stackrel{*}{\omega}_g^2) + \stackrel{*}{\omega}_z^2 \right\}$$

$$\stackrel{*}{\omega}_r^2 = 2\omega_r \stackrel{*}{\omega}_r = 2 \frac{\omega_r \omega_z}{\gamma} \frac{d\omega_r}{dz}$$

$$= \frac{2\omega_z}{\gamma} \left\{ \frac{\omega_r}{\omega_z} \left\{ \frac{\gamma^2 \psi^2}{R^3} - \frac{R}{r \gamma} \frac{\partial p}{\partial r} \right\} + \frac{\gamma \omega_r^2}{\omega_z} (\ln \gamma)^* \right\}$$

$$\stackrel{*}{\omega}_g^2 = 2\omega_g \stackrel{*}{\omega}_g = \frac{2\gamma \psi^2}{R^2} \left(\stackrel{*}{\gamma} - \frac{\omega_r}{R} \right) = \frac{2\gamma^2 \psi^2}{R^2} \left((\ln \gamma)^* - \frac{\omega_r}{\gamma R} \right)$$

$$\stackrel{*}{\omega}_z^2 = 2\omega_z \stackrel{*}{\omega}_z = \frac{2\omega_z^2}{\gamma} \frac{d\omega_z}{dz} = \frac{2\omega_z}{\gamma} \left\{ -\frac{1}{\gamma} \frac{\partial p}{\partial z} + \omega_z \gamma (\ln \gamma)^* \right\}$$

(7)

$$\begin{aligned} \omega_r^2 + \omega_\varphi^2 &= 2 \frac{\omega_r \gamma \psi^2}{R^3} - 2 \frac{\omega_r R}{\gamma r \delta} \frac{\partial p}{\partial r} + 2 \omega_r^2 (\ln \delta)^* \\ &\quad + 2 \frac{\gamma^2 \psi^2}{R^2} (\ln \delta)^* - 2 \frac{\gamma \omega_r \psi^2}{R^3} \\ &= 2 (\ln \delta)^* \left\{ \omega_r^2 + \frac{\gamma^2 \psi^2}{R^2} \right\} - \frac{2 \omega_r}{\gamma \delta} \left(\frac{R}{r} \right) \frac{\partial p}{\partial r} \end{aligned}$$

$$\left(\frac{r}{R} \right)^2 (\omega_r^2 + \omega_\varphi^2) = 2 (\ln \delta)^* \left\{ \left(\frac{r}{R} \right)^2 \omega_r^2 + \frac{\gamma^2 \psi^2 r^2}{R^4} \right\} - \frac{2 \omega_r}{\gamma \delta} \left(\frac{r}{R} \right) \frac{\partial p}{\partial r}$$

$$\omega_3^2 = 2 \omega_3^2 (\ln \delta)^* - \frac{2 \omega_3}{\gamma \delta} \frac{\partial p}{\partial \beta}$$

$$\begin{aligned} (\ln \delta)^* &= \frac{1}{2 c^2 \gamma^2} \left\{ 2 (\ln \delta)^* \left\{ \omega_3^2 + \left(\frac{r}{R} \right)^2 \omega_r^2 + \frac{\gamma^2 \psi^2 r^2}{R^4} \right\} \right. \\ &\quad \left. - \frac{2}{\gamma \delta} \left\{ \omega_3 \frac{\partial p}{\partial \beta} + \omega_r \left(\frac{r}{R} \right) \frac{\partial p}{\partial r} \right\} \right\}. \end{aligned}$$

$$(\ln \delta)^* = -(\ln \xi)^*$$

$$\begin{aligned} &= - \frac{\chi}{\gamma \delta} \left\{ \omega_3 \frac{\partial p}{\partial \beta} + \omega_r \left(\frac{r}{R} \right) \frac{\partial p}{\partial r} \right\} \\ &\quad \overline{\chi \left\{ c^2 \gamma^2 - \omega_3^2 - \left(\frac{r}{R} \right)^2 \omega_r^2 - \frac{\gamma^2 \psi^2 r^2}{R^4} \right\}} \end{aligned}$$

$$\delta (\ln \xi)^* = -\delta^*$$

$$\begin{aligned} &= \underline{\omega_3 \frac{\partial p}{\partial \beta} + \omega_r \left(\frac{r}{R} \right) \frac{\partial p}{\partial r}} \\ &\quad \underline{c^2 \gamma^2 \delta - \delta \left(\omega_3^2 + \left(\frac{r}{R} \right)^2 \omega_r^2 + \frac{\gamma^2 \psi^2 r^2}{R^4} \right)} \end{aligned}$$

$$\begin{aligned} \therefore \gamma(\ln \xi)^* = -\gamma^* &= \frac{\omega_3 \left\{ \frac{\partial p}{\partial z} + \left(\frac{r}{R}\right) \frac{dR}{dz} \frac{\partial p}{\partial r} \right\}}{\delta \left(c^2 \gamma^2 - (\omega_3^2 + \left(\frac{r}{R}\right)^2 \omega_r^2 + \gamma^2 \psi^2 r^2) \right)} \\ &= \frac{\omega_3}{c^2 \delta} \left\{ \frac{\partial p}{\partial z} + \left(\frac{r}{R}\right) \frac{dR}{dz} \frac{\partial p}{\partial r} \right\}. \end{aligned} \quad (12)$$

with (9) then

$$\gamma(\ln \xi)^* = -\gamma^* = \frac{\omega_3}{c^2 \delta} \left\{ \frac{dp_s}{dz} + \left(\frac{r}{R}\right)^2 \left(\frac{dp_E}{dz} - \frac{dp_s}{dz} \right) \right\} \quad (12)$$

Summary: Under the \mathcal{U} -similarity & (9) & $n = n(z)$:

$$\frac{dR}{dz} = \frac{\omega_r}{\omega_3}$$

$$\gamma_B^2 = 1 + \omega^2/c^2$$

$$\omega \varphi = \frac{\gamma \psi}{R}, \quad \psi^* = 0 \quad (\omega \varphi \neq \omega \varphi(\gamma))$$

$$\delta_B = \rho_i + p_E/c^2$$

$$\omega_r \frac{d\omega_r}{dz} \Big|_B = \frac{dR}{dz} \left\{ \frac{\gamma_B^2 \psi^2}{R^3} + 2 \frac{(p_s - p_E)}{\delta_B R} \right\} - \frac{\omega_r^2}{c^2 \delta_B} \frac{dp_E}{dz}$$

$$\omega_3 \frac{d\omega_3}{dz} \Big|_B = \frac{1}{\delta_B} \frac{2}{R} \frac{dR}{dz} (p_E - p_s) - \frac{1}{\delta_B} \left\{ 1 + \frac{\omega_3^2}{c^2} \right\} \frac{dp_E}{dz}$$

$$R^2 \omega_3 n = \text{const.}$$

Relativistic u -type jets cont:

Dick's
Notation
 \downarrow

$$r \equiv \frac{\tilde{\omega}}{R}$$

$$s \leftrightarrow l$$

In the stream-line formulation

$$u_z \frac{\partial}{\partial m} \neq \frac{u}{R} \frac{\partial}{\partial r},$$

but rather

$$u_z \frac{\partial}{\partial m} = \frac{u}{R} \frac{\partial}{\partial r} - u \tilde{\omega} \frac{\partial}{\partial s}$$

$$\text{Check: } \frac{u}{R} \frac{\partial r}{\partial r} = \frac{u}{R}$$

$$\text{Now } u \frac{\partial r}{\partial m} = \frac{u_z}{R} + \frac{u \tilde{\omega}}{R^2} \tilde{\omega} \frac{dR}{dz}$$

$$\therefore u_z \frac{\partial r}{\partial m} = \frac{u_z^2}{uR} + \frac{\tilde{\omega} u_z u \tilde{\omega}}{uR^2} \frac{dR}{dz}$$

$$\text{and } u \frac{\partial r}{\partial s} = \frac{u \tilde{\omega}}{R} - \frac{u_z \tilde{\omega}}{R^2} \frac{dR}{dz}$$

$$\therefore u \tilde{\omega} \frac{\partial r}{\partial s} = \frac{u \tilde{\omega}^2}{uR} - \frac{\tilde{\omega} u \tilde{\omega} u_z dR}{uR^2} \frac{dR}{dz}$$

$$\therefore u_z \frac{\partial r}{\partial m} + u \tilde{\omega} \frac{\partial r}{\partial s} = \frac{u}{R}.$$

$$\text{Now } w_3^2 \frac{d}{dz} \left(\frac{u \tilde{\omega}}{w_3} \right) = \frac{\gamma^2 l_s^2}{R^3} - \frac{1}{rnhc^2} \frac{u}{u_z} \frac{\partial p}{\partial m}$$

$$= \frac{\gamma^2 l_s^2}{R^3} - \underbrace{\frac{1}{rnhc^2} \left(\frac{u}{u_z} \right)^2 \frac{1}{R} \frac{\partial p}{\partial r}}_{①} + \underbrace{\frac{u u \tilde{\omega}}{rnhc^2 u_z^2} \frac{\partial p}{\partial s}}_{②}$$

(2)

$$\textcircled{1} = -\frac{1}{rhc^2} \left(\frac{u}{u_3}\right)^2 \left(\frac{2r}{R}\right) (p_E - p_s) = \frac{2(p_s - p_E)}{nhc^2 R} \left(1 + \left(\frac{u\tilde{w}}{u_3}\right)^2\right)$$

$$\begin{aligned} \textcircled{2} \Rightarrow u \frac{\partial p}{\partial z} &= u\tilde{w} \frac{\partial p}{\partial \tilde{w}} + u_3 \frac{\partial p}{\partial z} \\ &= 2 \frac{u\tilde{w}}{R} r (p_E - p_s) + u_3 \left\{ \frac{dp_s}{dz} + r^2 \left(\frac{dp_E}{dz} - \frac{dp_s}{dz} \right) \right. \\ &\quad \left. - \frac{2r^2}{R} \frac{dR}{dz} (p_E - p_s) \right\}. \end{aligned}$$

On the boundary; $\frac{dR}{dz} = \frac{\tilde{w}\tilde{w}}{u_3}$, $\textcircled{1} = \frac{2(p_s - p_E)}{nhc^2 R} \left(1 + \left(\frac{dR}{dz}\right)^2\right)$,

$$\textcircled{2} = u_3 \frac{dp_E}{dz}. \text{ Hence, on } \underline{\text{the boundary}}$$

$$w_3^2 \frac{d^2 R}{dz^2} = \frac{r^2 l_s^2}{R^3} + \frac{2(p_s - p_E)}{(nhc^2 R)} \left(1 + \left(\frac{dR}{dz}\right)^2\right) + \frac{1}{(nhc^2 R)} \left(\frac{dR}{dz}\right) \frac{dp}{dz}$$

This is the same boundary eqn. as obtained by the other approach ($(nh)_B c^2 \equiv \delta_B$, $l_s \equiv \psi_s$).

As indicated prev. the extra term (pressure gradient) for an 'ideal' gas gives

$$\sim \frac{c^2}{T} \frac{dT}{dz} \frac{dR}{dz} \quad \text{for} \quad \frac{c^2}{T} \ll k/m$$

the relativistic component, but

$$\sim -\frac{3c^2}{T} \frac{dT}{dz} \frac{dR}{dz} \quad \text{for} \quad \frac{c^2}{T} \gg k/m$$

the 'thermal' component.

k/m
 $\sim 10^{-11}$ "elect."
 $\sim 10^{-8}$ "prot."
 c^2/see^2
 $m_e c^2 \sim 10^{10}$ "el."
 $\frac{k}{e} \sim 10^{-3}$ "P."