

Obvious mechanical advantage of transit instruments. Difficulty is in N-S aperture. To $2 \times$ ap must then $\frac{1}{2} \lambda \rightarrow$ only $\sqrt{2}$ in S:N.

Nearly-transit observations (e.g. Puerto Rico dish) \rightarrow cannot track arbitrary objects without mirroring bits of sky in between \rightarrow makes obs. programme untidy.

Astronomical Problems

These still determine extent to which design features are compromised.

Galaxy. Most of it resolvable $30' - 60'$ beam. No pointing need for "resol".

Solar. No sensitivity problem. No multiplicity problem, can use gratings.

Sources.

① Obs. on range of $\lambda \rightarrow$ spectra of features.

② Shortest pos. $\lambda \rightarrow$ accurate positions, λ^r structure.

③ Optimum $\lambda \rightarrow$ weakest pos. sources perhaps.

3 types.
of programme

\downarrow S:N ratio, seeing source clear of weaker ones behind it

② can \rightarrow S:N problem too, if weaker sources are of interest. Or extended sources with low Tb.



Also versatility of instrument. Must think of future

Radar. Repts. are v. different. $S:N \propto \frac{P_{transm.} G. A_{collect.}}{T_{sys}} \sim \frac{PA^2}{\lambda^2 T_R}$

Considerable advantage of small λ , or perhaps more realistically on P/λ^2 . Radar needs different criteria, & radar suitability \neq radio suitability. Also only a handful of objects of study, so antennae must be steerable so as not to waste time. Paraboloid is good for this.

② \rightarrow $10''$ arc of interest now.

Fighting against "chance" identifications. Asymmetry not important @ $1' \times 1'$, say.

$\sim 5''$ arc accuracy of finding radio pos. on a sky chart is realistic. Now asymmetry is important & do want a pencil beam. Otherwise "chance" identifications of weak sources (dishes) do not mean v. much   Areas v. differently increased by "finding error".

Near normal galaxies. low Tb. Difficult \because flux/beamwidth small. M31 needs $< 1''$ for structure. Can sacrifice a little in resol. but sensitivity problem is acute.

Radio galaxies. Less problem pointing.

Spectra. Extend CK in δ and ν . Study red-shift effects, evolution perhaps.

LF. Doppler irregularities limit resolution for given instrument.

HF. Situation far away is different from $\log N - \log S$. Luminosity fn. wanted.

Fundamental difficulty. Low P obs. are local. High P obs. are distant.

\therefore cannot construct luminosity fn. $f(P)$, seeing as $\log N - \log S$ is so odd.

Have constraints too, e.g. integrated emission. May be resolvable!

Might be worth getting distances done, irrespective of spectrum. Accept best compromise to get weakest poss. sources. Strong case for this at present.

What are the fundamental limitations? No electronics, no cash problem.

- i) Noise from sky, ground.
- ii) Must choose thin ionosphere. Irregular structure \rightarrow scintillation $\sim 3-30$ sec. @ night
- iii) Solar wind @ daytime \rightarrow trouble here. λ delobe problem.
- iv) ~ 100 km \rightarrow dens. of source from $\sim 5''$ of time. longer than τ .
 $178. \Sigma \phi \sim 10 \rightarrow 15^\circ$. A.H. based needles $\sim 25\% / \sqrt{25}$ for 25 points $\rightarrow 5\%$.
 FUNDAMENTAL trouble. Need primary noise? better.
 Wave reflection. Can be corrected by ionospheric soundings. Sumpst min. it's ok.
 limits you to $\sim 5000/\lambda$ metres.

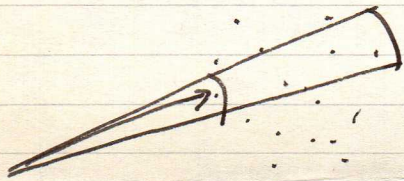
38 mway $\rightarrow S_{118} \sim 3$ fu. limited by $re \ 500/\lambda$ rel? in fact.
 81.5 $\rightarrow 16 \times$ worse? would $\rightarrow S \sim 0.5$ fu.
 408 $\rightarrow 8$ km telescopes!

1) Rx $\rightarrow T_R + T_{gal} + T_{arm} + T_{no} \rightarrow$ Total system noise. (Thinking 1 source + Background + Galaxy)

$$\Delta T_a \text{ detectable} \sim \frac{1}{\sqrt{B\tau}} T_{total}$$

$$\frac{1}{2} SA \text{ must be } 10 \times T_{total} \cdot \frac{1}{\sqrt{B\tau}} \text{ or less.}$$

Other limit. No noise, no galaxy, etc, but uniform pop.



If so ~ 3.1 times further out, sources are 10% less S.
 \rightarrow 10% error in the flux of foreground source. Then no. of sources / beams \rightarrow limiting so for $\frac{1}{10} S_0$ accuracy.

This or $\rightarrow 27$ beam areas / source. $<$ this \rightarrow source $>$ 10% with appreciable probability.

$$N/\text{star usefully observable} \sim \frac{1}{30} A/\lambda^2 \text{ from this.}$$

Difficult to work out confusion lt. precisely.

But P(D) approach \rightarrow this problem from data explicitly gov.

Tells us that $D \sim 1.5 - 2 \times S$ of faintest source in beam.

Statistical, tho, no some sources will be in considerable error.

D is like an S, but takes acct. of fact that sources are modified by beam shape if sampled just @ non-redundant rate.

If D_{max} is sig? $>$ noise on record, then info. from P(D) is useful.

\rightarrow source statistics, but not individually identifiable ones.

\therefore for this, it is well worth being highly confusion limited.

Also pos. error. \perp scanned wire $\Lambda \rightarrow \Lambda$
 $\text{FW} \sim 10\% \text{ range } \frac{1}{2} \text{ beams away} \rightarrow \approx 10\% \text{ pos. error.}$

To go up $\times 10$ in distance. Area of collecting $\times 100$
 resolvable $\times 1000$.

limitations set by confusion predominates in bigger arrays.

"Effective areas."
 i) $\omega = \lambda^2/A$ Resolving power. Resolving area \neq Physical.
 ii) Normalized collecting area, by S:N of conventional instrument of same actual area.

Discuss \equiv res on area basis. If looking @ resolvable sources, "driving time" is important. Area \equiv res , not the whole story. If surveys, areas are the thing. Multiple beaming using Rx complexes also adjusts these comparisons.

Limiting Effects of S:N & Confusion.

Consider paraboloid \because it's simplest.

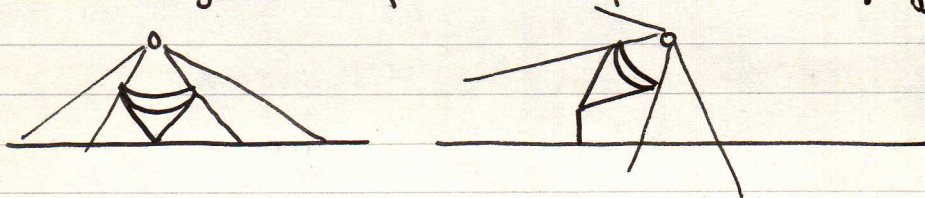
T_R set by Rx \rightarrow not a fn. of paraboloid.

Assume 1st stage is @ focus, no loss.

primary feed perfect to \rightarrow ideal illumination. Note, this \neq uniform illumination. \therefore this \rightarrow appreciable overspill $\&$ ground detection. If grade it too much to \rightarrow no overspill, lose effective gain of system. \therefore Compromise.

$$\frac{1}{G} (T_R + T_{gal} + T_{gs}) \rightarrow \text{system noise}$$

Cannot throw away T_{gs} wily far \because this $\rightarrow G > \&$ syst. noise eventually $<$.
 Got to be careful with overspill when working off zenith.



$S_{10} - 1000 \text{ Mc/s}$. Broad min $T_R \sim 80^\circ - 100^\circ$ over all angles. LF LF. is Galaxy.

Can improve this by keeping on zenith, masers, etc.

in 1955, the min was $\sim 200 \text{ Mc/s}$. $\therefore 178$

1964

$S_{10} - 1000$

$\therefore 408 \& 1420!$

} closest approach to 0.7 spectrum.

$$\Delta T_n = \frac{1}{\sqrt{B}} (T_R + T_{gal} + T_{gs} + \dots)$$

Consider $B \sim 10 \text{ Mc} = 10^7$

i.e. $B \text{ Mc/s } \tau_1$

$\tau_1 \text{ Mc/s } \tau_{10}, \text{ say.}$

T_{gs} , scanning rate.

B set by freq. cell:

408 5 Mc/s
 1420 27 Mc/s

Get ΔT_n min @ $\lambda 50 \text{ cm}$. in feet.

Now ΔT_{conf} ? Minimise $\Delta T_n + \Delta T_c$. \rightarrow optimum \forall for telescope 1964.5!

For given dish, can plot ΔT_c vs. ν (allowing for spectrum).

100m $\Delta T_c + \Delta T_n$ min @ 16cm. Note that this dep. on B, τ , etc.

\uparrow

awkward to work precisely, as it knows in advance what $\log N - \log S$ is

In fact, on best guess about source ct's., all sizes of instrument optimized $\sim \lambda/25\text{cm}$.
 \therefore Any instrument, whatever the size, best $\sim 25\text{cm}$. for minimum noise T/ccl.

Again, remember that B & T fixed in this calcⁿ.

B & T limited in various ways, tho, & even \rightarrow range available $\rightarrow 15-30\text{cm}$ perhaps.

Not true that 1000' dish with 3cm maser is the best. 1000', yes, but 21cm!

Fallacy is in source ct's., perhaps, or not clear, for 0.7 spectrum of sources.

Dish 1000' @ 21cm. still not v. good resⁿ? tho!

Structural problems. Queso-connected structures, gravity loading might be avoided
 (loop wind troubles!

\downarrow
 of adequate complexity, $P_{\text{net}} \sim$ several orders. Will have trouble with wind. Just structure $< 1\text{sec}$. Cannot stabilize this $< P_{\text{net}}$, except using huge powers for rapid acceleration. 1 MW to run telescope! Can stab. against gravity loading tho, but this isn't always the main one.

Mezco. pretty good in most respects. Sphero forms full aperture, but this means overfill unimportant. All that happens is beam degradation.

But its beam is not ideal for source structure.

Unfilled apertures are more versatile.

For them, can get better resⁿ? $\rightarrow \Delta T_c$ limits $>$.

Possibility of working on longer $\lambda \rightarrow$ less structural problems, \therefore bigger instr.,
 \therefore , up to a point better ΔT_c !!

This eventually converges of course, but shows that synthesis can well afford to go to higher wavelengths than brute force parabolics!

1.8 used \neq @ $\Delta T_N \sim \frac{1}{3} \Delta T_c$. O.K. for us \therefore we have PCD methods.

\downarrow
 not opt. \therefore 1.8 slope used on longer than $3\lambda \Rightarrow$
 $+ \text{presump improved greatly.}$

Fix collecting area & juggle with shapes \rightarrow unfilled apertures.

S:N same, but ΔT_c much less \therefore of better resⁿ. Balance bet. resⁿ & S:N shifts to higher λ .

A point.
 "Filling factor" = $A_{\text{res}} / A_{\text{col}}$

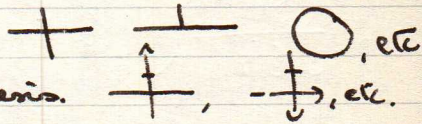
Resⁿ $\rightarrow \Delta T_c$. Choose collecting area o.r. $\Delta T_N \sim \Delta T_c$ (not using PCD).

make $\Delta T_N > \Delta T_c$ if PCD also to be used.

2 Distinct classes of unfilled instrument.

i) all elements physically present \rightarrow electrical systems

ii) not or once \rightarrow computer systems.



All systems \approx same in S:N for given area of sky & observing time, see A.H. lectures.

300m dish $\rightarrow 1' @ 5m$.

@ 25m, collecting area can be down by $\sim 1/4$
filling factor $\sim .290!$

Design to receiving power. Get sensitivity req. later, not knowing time / beamwidth involved.
At high. resolen., always the unknown factor of cosmology. Have to guess eventually.

Atoms in two classes. i) Well resolved. T_{surf} small, not much S / beam area
ii) Not resolved or only just. T_s great, plenty of S / beam area.

4c 30' x 20' 600 / Xer @ 2 f.u.

Suppose want 10^5 / ster, ~ 1 source / 30 beam areas. Want $\therefore \sim 2' \times 2'$

300m dish, $\lambda 10cm$.

Sensitivity? We'll guess $N \sim S^{-1.0} \rightarrow -1.5$

$$S_{ms} \sim 0.01 \text{ f.u. ray.}$$

$$S_{3000} \sim .001$$

$$\text{Aerial temp } \sigma, kT_A = \frac{1}{2} SA \sim \frac{1}{2} \times .001 \times 10^{-26} \times .6 \times \pi \times 2.25 \times 10^8 \rightarrow 2 \cdot 10^{-24} \text{ K}$$

↑
efficiency of paraboloid.

Suppose want to see such a source with S:N of 5 (forget const. for mt.)

$T_{\text{rept.}} 100$ rays. SW 10m/ps.

$$\text{Want fluct.} \sim \frac{1}{\sqrt{10^2 T}} \times 100 = 4 \cdot 10^{-3} \quad \tau \sim 70 \text{ sec.}$$

Must wait this long / ~~beam~~ ^{no.}

Want ~ 4 nos. / beam in each dir. ~ 16 nos / beam area.

Want $\sim 4\%$ / beam area. $\rightarrow 280$ sec / beam area.

(Different if you know where sources are, this is for surveys, where we don't & must wait)

Fully-filled sp. \square^D . 100% (Not \odot D, note. This has less area & small efficiency). ^(.6) ①

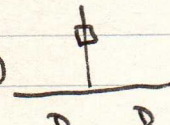
Synthesis \square^D $\frac{1}{\lambda} \frac{1}{d} \frac{1}{d}$. D lag ③


T $\frac{D}{D} \frac{1}{\lambda}$ ②

① $S/N \sim D^2$

② $\sim 2\sqrt{Dd} \cdot \sqrt{2Dd}$ Quad: $\rightarrow 3Dd$

③ $2Dd \cdot \sqrt{D/d}$ \rightarrow (3) $D^{3/2} d^{1/2}$

④  $S/N \sim 2\sqrt{2Dd \cdot d^2} \sqrt{D/d} \rightarrow 3Dd$

⑤  $2d^2 \sqrt{\frac{2D^2}{d^2}} \rightarrow 3Dd$

What sort of vals. of d/D wanted? 300m @ 10cm. the criterion, remember 280 sec/beam.


On $\lambda 40cm \rightarrow 4 \times$ area filled. S:N 3:1


D 1000m., $3Dd \sim \frac{1}{3} 4 \cdot 10^4$ $\therefore d/D \sim 1/2\%$ o.k.

Quite narrow arms, then, given same τ obs & same S:N, optimising λ each time.


Earth rot:

① Transit instruments. T style Rx Scan by earth rot:
 T must be set by this. $\sim \frac{1}{4} \cdot \frac{\lambda}{D} \times 24 \times 3600 \text{ sec.}$
 Per beam area, speed $\sim 4T \therefore$ must scan strips not more than $\frac{1}{4}$ beamwidth apart.


②  $4T$ again.

③  $4T$. Essentially very similar.

~~These~~ all of these give long thin strips of sky. Nothing can be done about this.

④  \rightarrow Can run the little one along long run @ $\sim d/T$. Need only speed T in each pos.

Every source remains in reception pattern for longer time (λ/d comes in, not λ/D).
 \therefore Effective T is increased from T to $\frac{D}{d} \times T$. This \rightarrow same as before now.

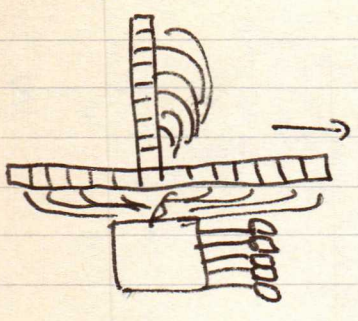
⑤  \rightarrow successive 24-hr pos? for each pos. of other one.
 Can use $T \sim \frac{1}{4} \frac{\lambda}{d} \times 24 \text{ hrs.}$

S:N $\sqrt{\frac{D}{d}}$ better, obs. time $<$ though, by $\frac{D}{d}$, \therefore S:N better by $\sqrt{\text{obs. time}}$.

④ & ⑤ are 2 extremes of 2-d systems.
 Extreme cases of sensitivity & obs. time.
 ⑤ is inconvenient \therefore of amount of data. Must do all sky virtually.

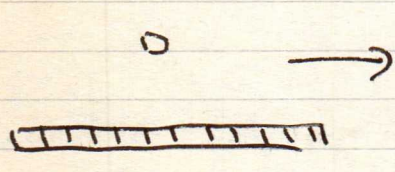
hence interferometry. Has to do a selected area of sky by ⑤ in effect.

Multiple receivers.



Observation rate bettered.
 \downarrow
 Beam NS arm \rightarrow diff declinations.
 E-W arm \rightarrow better S:N by \sqrt{N} where N Rxs used.
 No betterment in the scanning time.

This sort of technique makes the large semi-filled arrays worth considering seriously.



Simultaneous systems. In a complete SN $d^2 \sqrt{N} \sqrt{DT/d}$
 or multi-beaming. complete & join. $\sqrt{d^2 D N T}$

- Difficulty of multiple beaming is:
- i) future rate
 - ii) cost - must use poorer quality individual elements
 - iii) vertical Rtx \rightarrow bigger aerial etc / channel \rightarrow & bigger.
- 1-Rx systems easily breaks even or not of this.

Supernovae.

i) S.N. good \because of long tracking time / bit of sky.

ii) ~~1-d systems~~ 1-d systems cpr. done for you by Earth rot? Time fixed @ 12h.

Limited in this respect.

Geometry P.A. O'Brien M.N. 113, 5 (1953). Solar work. v. first of syn.

EW or NS? Want to avoid low δ \because of atmospheric effects.

Really need 2 of them to get full coverage, with N-S vert. as well.

Trouble with sidelobes if use a 2-way mock-up. O.K. for Sun, but not for a deep survey.

NS.

Must have complete Δ syst. if leave out some \sphericalangle , then get -ve pattern of ∞
This has vert. one way but not other \rightarrow Needs of opacity across the field. Not work
it. Could overcome by grading but this degrades the area for res. & S.N.

Settle for EW one

ACN 1960. N-pole with 178 to obviate tracking. $\sim 4^\circ$ diameter.

\rightarrow more or less symmetrical beam \because box used \sim rectangular.

Inevitable moving by distance = d , not the best $2d/3$. \therefore Not getting overlap.

O.K. for centre of map, but cannot move out far off primary beam.

Strong source near edge of beam showed up sidelobe effect.

Perhaps even a little better than ought to have been expected \because the aerial els. were all different "may not be perfectly phased"!

Final Syn. Circular area out every 100 days. Total survey time same as any \perp -system

Saving in steelwork.

Travel speed on rail track reasonable.

Practical Points.

i) Away from N-pole. Tracking instruments worked. Expensive if large.

ii) Bandwidth effects. Need $\sim 1/2$ of equality of paths.

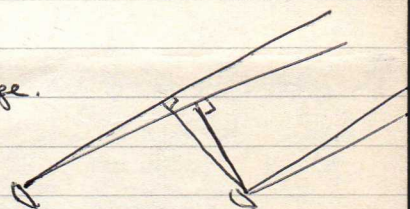
Even the Δ obs. limited by this

Sky @ edge of beam \rightarrow attenuated interference pattern.

Diff. of para band Δf .

Need to ensure that $\Delta f/f < d/D$. not to run into this effect.

Want to balance the conditions really. Can get sidelobe appearance this way. Checked carefully tho as it turns out to be res. for attenuated Δf .



Sidelobe Response.

DA, $\Delta\phi$ per unit. Can stand 20% DA \equiv 10% $\Delta\phi$.

$\% \Delta\phi$ / perm is $\times 90$, total sidelobe level is $\sim \frac{1}{\sqrt{N}} \times 90$.

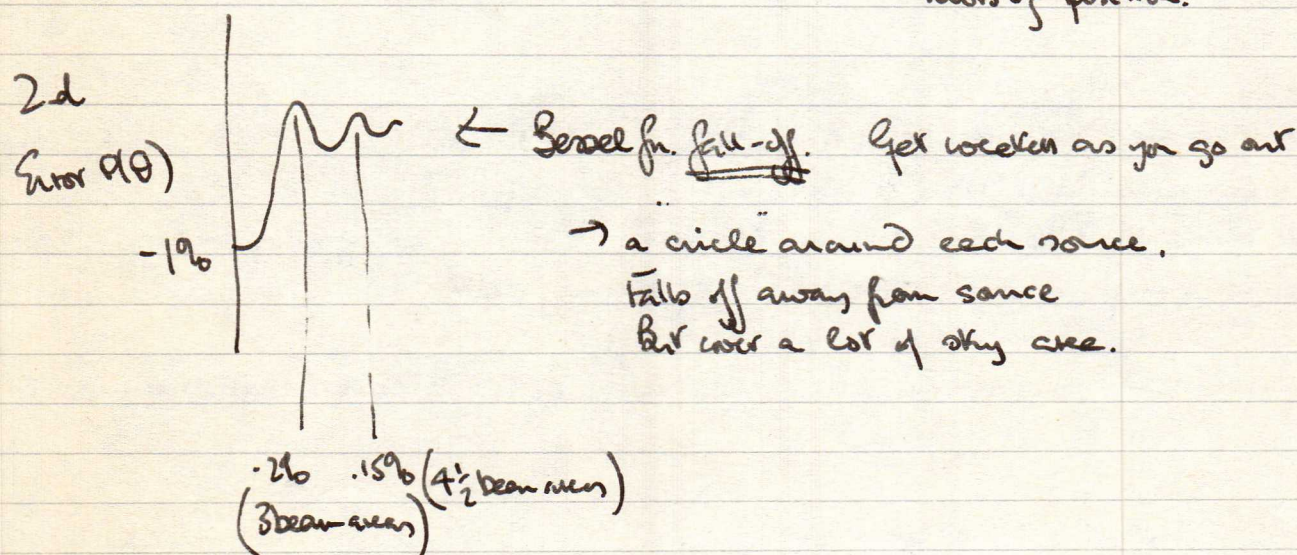
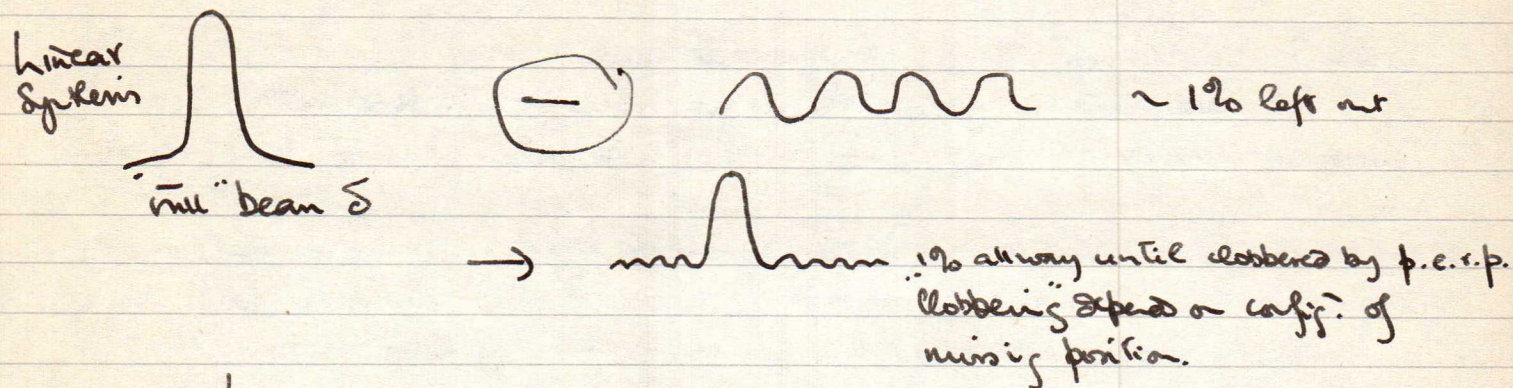
Calibration sources take out bias $\Delta\phi$ (Rx) from time to time.

Much easier to get @ $\Delta\phi$ if only 2 els. If 110 els, no intrinsic problems of ϕ tracking, but the complexity of feeder system makes it difficult in practice.

— Not so easy with Mills + wire ~~ant~~ the long beam is narrow. May not see an intense S every day

Short-term $\Delta\phi$ not so important in 2-d systems \therefore the no. of points is eff. much larger.
 of 10 points 1-d \rightarrow 100 2-d $\&$ ~ 10 -factor in the sidelobe level due to $\Delta\phi$
variance (cancel minus, rather than 24 hrs!)
 \hookrightarrow cable changing.

Suppose 1 pos. left out, for 100 points.



Which is really more important. Linear const. amp, const area lobes, or Bessel modulated increasing area lobes, ultimately depend on $N(S)$. If $N \sim S^{-1.0}$, then there is not much in it. If $N \sim S^{-1.0}$, Bessel sidelobes are preferable.

Incomplete path compensation.

Suppose all left uncompensated

$$\frac{2\pi dL}{c} (\Delta f) = \Delta\phi \text{ across BW.}$$

If this $\Delta\phi$ got to 2π , no record at all!

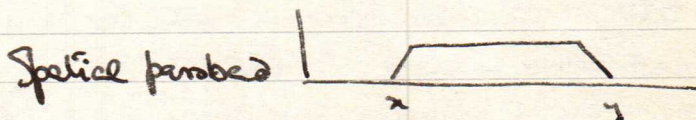
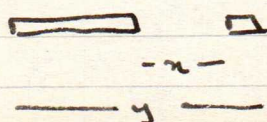
Must make dL v. much less than d or $\Delta\phi \rightarrow 2\pi$. Not dep. on f , only Δf .

long reception pattern $\Delta\theta$. $L \cos \theta - L \cos(\theta + \Delta\theta) < c/\Delta f$ $L = \text{instr. spacing.}$

$$D/d < f/\Delta f.$$

Sampling rate. May have to get rid of interference pattern to reduce sample rate. Can do this by further path compensation.

178

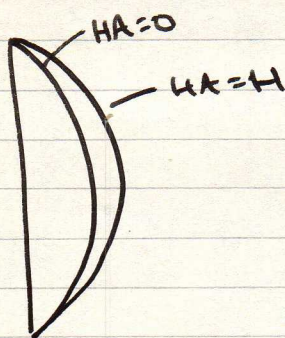
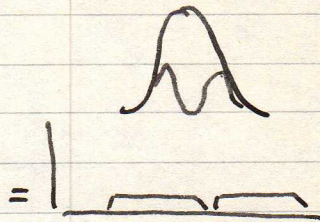


\rightarrow freq. response as Sawtooth notches.

→ *W* record, not *MM*.

Blinded yet again: $\Delta\delta$ in the lary beam & the "quasi-period" of the fringes is any way $\sim \tau \approx \delta$.

McAdam. low Culmination above at high δ .
inter of p interference pattern & get 2
 narrower responses.



$$\phi = \frac{2\pi h}{\lambda} \cos\delta \sin H$$

$$f = \frac{d\phi}{dt} = \frac{2\pi h \Omega}{\lambda} \cos\delta \cos H$$

P.d. to 2 slant
 acids.

$$\Omega = \text{Earth.}$$

$$= 0 \text{ for } H = 6^\circ, 18^\circ$$

$$\frac{df}{dH} \equiv \left[\frac{df}{d\alpha} \right] = \frac{2\pi h \Omega}{\lambda} \cos\delta \sin H$$

$$\frac{df}{d\delta} \rightarrow \frac{2\pi h \Omega}{\lambda} \sin\delta \cos H$$

$HA = \pm 6^\circ$, No var. with δ .

$$\frac{df}{dH} = \frac{2\pi h \Omega}{\lambda} \cos\delta \quad (\text{SH})$$

$$= \frac{2\pi h \Omega}{\lambda} (\delta\theta) \text{ in } \text{km.}$$

$HA = 0^\circ$

$$\frac{df}{dH} = 0.$$

$$\frac{df}{d\delta} = \frac{2\pi h \Omega}{\lambda} \sin\delta \quad (\text{SH})$$

$$= \frac{2\pi h \Omega}{\lambda} \sin\delta (\delta\theta) \text{ in } \text{km.}$$

Must sample @ rate $\sim \frac{\lambda}{2\pi h \Omega \delta\theta}$.

Nothing can be done a record faster
 than this.

$\sin\delta$ depce of course \equiv to decrease aperture with δ . Area $\sim A_0 \sin\delta$.

Benelux. MKI ended up as Bologna, versions 1-2.

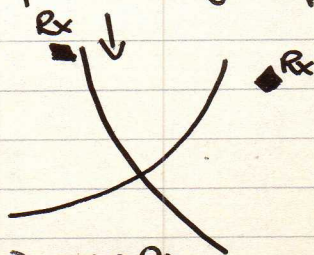
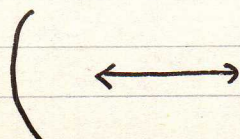
Mills New +

Benelux II, IIa, III

van Hoerner $d/d(\cos\theta)$ approach - Cross-type telescope but with feeder problem lessened.

I.R.T. USSR proposal.

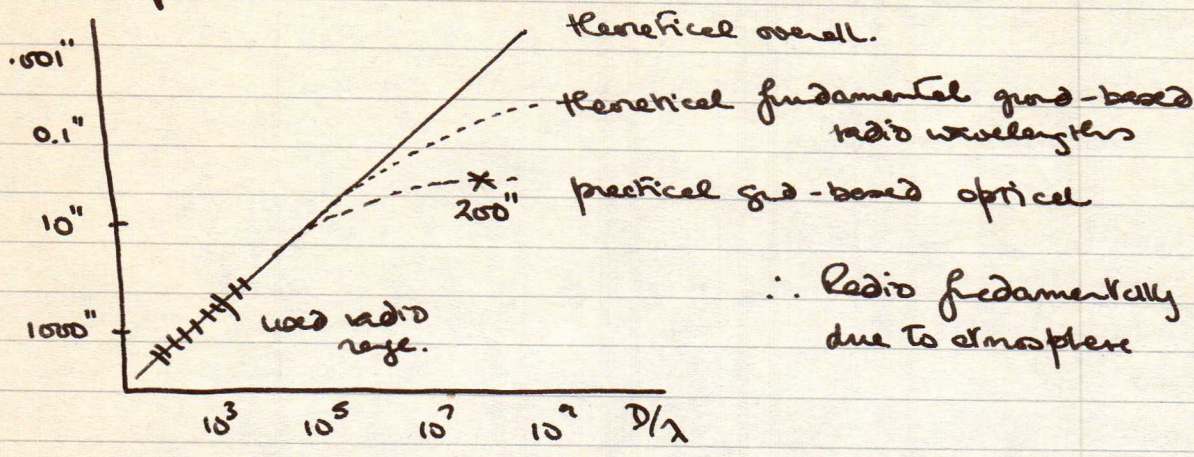
Pulkova.



Wood!
 + glue!

To scan need diff. focal lengths. Up the reflector \rightarrow move Rx.

I.R.T. report

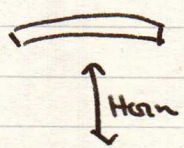


∴ Radio fundamentally better due to atmosphere

1-3" resolution? + sensitivity.
Sens. reqd. → cosmology again.
Considered



flat surfaces



Horn

approach

Why not come to mean focal length?

Resolution 1-way only @ low elevation.

What are sidelobe responses?

Air path for placing the array. May be better than cables.

For low λ, worry perhaps about air losses, & also air radiation.

Ought to be more worried about primary horn pattern. Spill-over → a cost of grid.

~ parameters considered R ~ 10km

~ 500 panels, ht ~ 100m width ~ 30m grid reqd.

BW → 1" @ 10cm.

→ 10⁹ galaxies (has an ε does he know?)

~ 3.10⁶ tons + 500 2-d accurate gearboxes.

M.R. estimates min pars £500/ton. Each d ~ 1 J.B.! → £1.5 x 10⁹.

Only need 1 Rx!

Difficult to use more than one Rx, & get any rapid scanning or Rx-based economy.

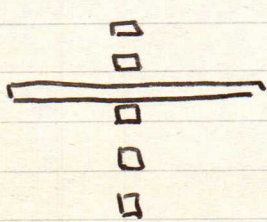
Miles +. Cyl. par. Arms 1600m ~ 13m wide 408 x 111 mpts.
2.8' 10'

$$D = 800m, d = 13m$$

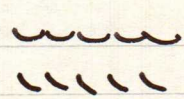
Apple Rx. Perhaps distrib. 177 + 22 xtd mixers.

$$S:N = \frac{3 \times 4 \times 800}{1000} \sqrt{N}$$

Benelux Ia



408



fully fills 1 cm a zenith all look @ each other

∴ ~ ~ ~ ~ one side other.

No info. cont. None redundant.

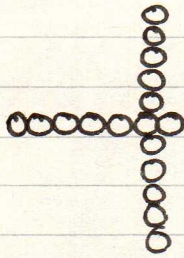
Expense over ed-Trievs. These are more expensive than middle ones, \therefore you want to cut down on construction: rigid somewhat with all this no. of them.
 Utilized gating responses from the \vdots ones, cut out by having a biased long one
 whose response \leftrightarrow trips them down. \vdots

Bologna $D \sim 600m$ Xcel mixers. S:N $\frac{3 \times 600 \times 35}{1000} \sqrt{N}$
 $d \sim 35m$ 108

Slightly better than Mills if N same. But Mills has N large.

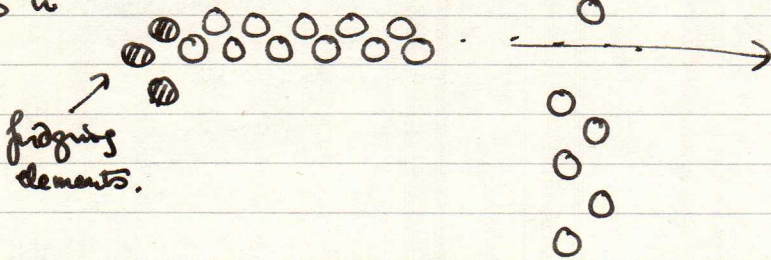
Benelux II.

Rethink. 21cm. instead of 408 mds? Cyl. per. out @ this λ .



not poss. \therefore Key kind.
 also not all arms filled.

Must go to



Middle? Flaw, but they worked it out, as it came to $\sim 7m$ paraboloid missing. \therefore build one of these elsewhere

Sensitivity was lacking though - very lucky.

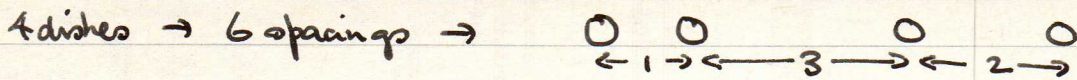
Try scanning a little way - it's deep. This \rightarrow bigger ζ .

~~But~~ but cut diverged faster than S:N was obtained.

Spermythesis considered.



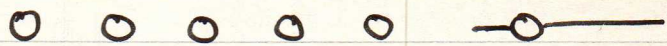
all scan. all pairs mutually joined.



Unfortunately this doesn't continue very far.

Cannot fill all gaps except by using one marble somewhere.

Benelux III.



Uneconomic of L's B. but it spreads faster.

1500m x 25m dishes. $\rightarrow f_{1.5} \times 10^5$

$D \sim 1500m$ $d \sim 25m$

Xcel mixers still to be used. Claim mixers $\sim 600^\circ K$ with low IF.

This throws away some of the factor gained got by 10 x dishes.

Paras $\sim 200^\circ K - 100^\circ K$ easily. 3 paras not too offiener.

Benelux better for detailed strong structure. i.e. where sensitivity important.
 Better \therefore faster. Takes $\frac{1}{6}$ time $\rightarrow \frac{1}{4}$ S:N.

If Benelux takes same time (looks @ all 6x) \rightarrow S:N 0.6.

Also they have not looked @ so much sky @ end.

\therefore They are missing it by not going far out to perantros.

As it is they'll only be better where S:N not important.