



# VLA OBSERVING APPLICATION

AB 3,46

received:

SEND TO: Director NRAO Edgemont Rd. Charlottesville, Va. 22901

DEADLINES: 15th of Mar., June, Sept., Dec. for Q 3, 4, 1, 2 respectively

① Date: 13 March 1985

② Title of Proposal: low-brightness features of NGC6251

③	Authors	Institution	Who will observe?	For Grad Students Only	
				Observations for PhD Thesis?	Anticipated PhD Year
	A.H. Bridle	NRAO / CV			
	R.A. Perley	NRAO / VLA			

④ Related previous VLA proposal number: AP66 (request for rescheduling of failed part of AP66)

⑤ Contact author for scheduling: R.A. Perley  
Address: VLA

⑥ Telephone:  
TWX:

⑦ Scientific category:  planetary,  solar,  stellar,  galactic,  extragalactic

⑧ Configuration(s) (A, B, C, D, A/B, B/C, C/D, Any)	D				
⑨ Wavelength (90 20 18 6 2 1.3 cm)	20/6				
⑩ Time requested (hours or days)	24hrs				

⑪ Type of observation:  mapping,  point source,  monitoring,  continuum,  in poln,  circ poln,  spectral line,  solar,  VLBI,  phased array,  other \_\_\_\_\_

⑫ ABSTRACT (do not write outside this space):

We wish to be rescheduled for the part of AP66 which failed due to operations problems with the VLA. The purpose is to examine the spectral gradients and Faraday rotation properties, as well as the magnetic field configuration over the low-brightness regions of the giant radio galaxy NGC6251. We also wish to test Haring's lobe magnetic field model for this source, and to understand why the S symmetry of the jet/counterjet does not extend eastwards in the

NRAO use only

Source.

13 Observing style:  Will be present  Will prepare files & return to reduce  Will use modem  Absentee (NRAO prepares OBSERV file & sends calibrated data)

14 Reduction: Number of maps 12 Maximum size of maps 512 Self-cal maps 12 Private disk pack \_\_\_\_\_

15 Off-site reduction:  none,  post map,  post calibration,  everything.

16 Help required:  none,  consultation,  friend (extensive help),  staff collaborator.

17 Spectral line only:

	line 1	line 2	line 3		line 1	line 2	line 3
transitions to be observed	_____	_____	_____	number of channels (N)	_____	_____	_____
channel bandwidth (KHz) ( $\Delta$ )	_____	_____	_____	number of antennas	_____	_____	_____
observing frequency ( $\pm \Delta/2$ )	_____	_____	_____	rms noise after 1 hour (mJy)	_____	_____	_____

18 Number of sources 1 (If more than 10 sources please attach list. If more than 30 give only selection criteria and LST range(s).)

Name	Epoch 1950 <input type="checkbox"/> 2000 <input type="checkbox"/>		Config.	Band (cm)	Band width (MHz)	Total Flux		Largest ang. size	Weakest signal (mJy/beam)	Required dynamic range	Possible LST range hh - hh	Time requested
	RA hh mm	Dec $\pm$ xx'x				line (Jy)	cont. (Jy)					
NGC6251 (3 subfields)	16 36	+82°7'	D	20,6	50/25			30'/10'	~0.1	4000:1	any	24 hrs

19 Special hardware, software, or operating requirements:

20 Preferred range of dates for scheduling:

21 Dates which are not acceptable:

22 Please attach a self-contained Scientific Justification not in excess of 1000 words.

When your proposal is scheduled, the contents of this cover sheet become public information. (Any supporting documents are for refereeing only)

NATIONAL RADIO ASTRONOMY OBSERVATORY  
Edgemont Road, Charlottesville

13 March 1985

TO: Paul Vanden Bout

FROM: Alan Bridle, Rick Perley

RE: Rescheduling of VLA D array observations of NGC6251

We wish to apply for rescheduling of the 'D' array segment of our proposal AP66 for mapping the low-brightness lobe features of NGC6251 at 6 and 20 cm with the VLA. This proposal was given time in the 'C' and 'D' array seasons in 1983 but the 'D' array observing was unsuccessful for operational reasons. To support the resubmission we attach the original proposal, and a map from the (successful) 'C' array observations.

AP66 called for 'C' array data mainly to define properties of the outer main jet, the counterjet and lobe fine structure, and 'D' array data mainly to define the spectral, polarization, and rotation measure characteristics over the extended lobe emission. We "piggybacked" an 18cm 'C' array run on a 28-hr VLB observation of NGC6251 which used the VLA in phased array mode; Figure 1 shows a tapered map from this run, at 25" resolution. It clearly demonstrates (a) that the two jets share a distorted S-symmetry, (b) that the counterjet is not a fainter replica of the main jet, but rather that the brightness ratio between the two jets changes with distance from the core, (c) that the "warm spot" in the west lobe shares the S-symmetry of the jet/counterjet system with a corresponding warm spot at a bend in the counterjet. The last result increases the importance of examining the magnetic and spectral properties of the extended emission to the east of the warm spot in the counterjet (Figure 2), as it is now much clearer that the most easterly emission in NGC6251 breaks an underlying S-symmetry in the source. The 'C' array 6cm data (required for better signal to noise on the main jet than achieved in our published work) were also of acceptable quality for our present purposes.

Unfortunately, the 'D' array data requested in AP66, taken in June 1983, are almost entirely useless. The observing run was scheduled just as the BD IFs were being brought into use. Due to various operational problems, the new BD channels were brought up with no delays set, and the AC channel delays were improperly determined. The result was that only the parallel-hand data were useful at 6cm, while at 20cm no valid data at all were obtained. We therefore request rescheduling of the 'D' array segment of this proposal for 12 hrs in the next 'D' array season.

DECLINATION

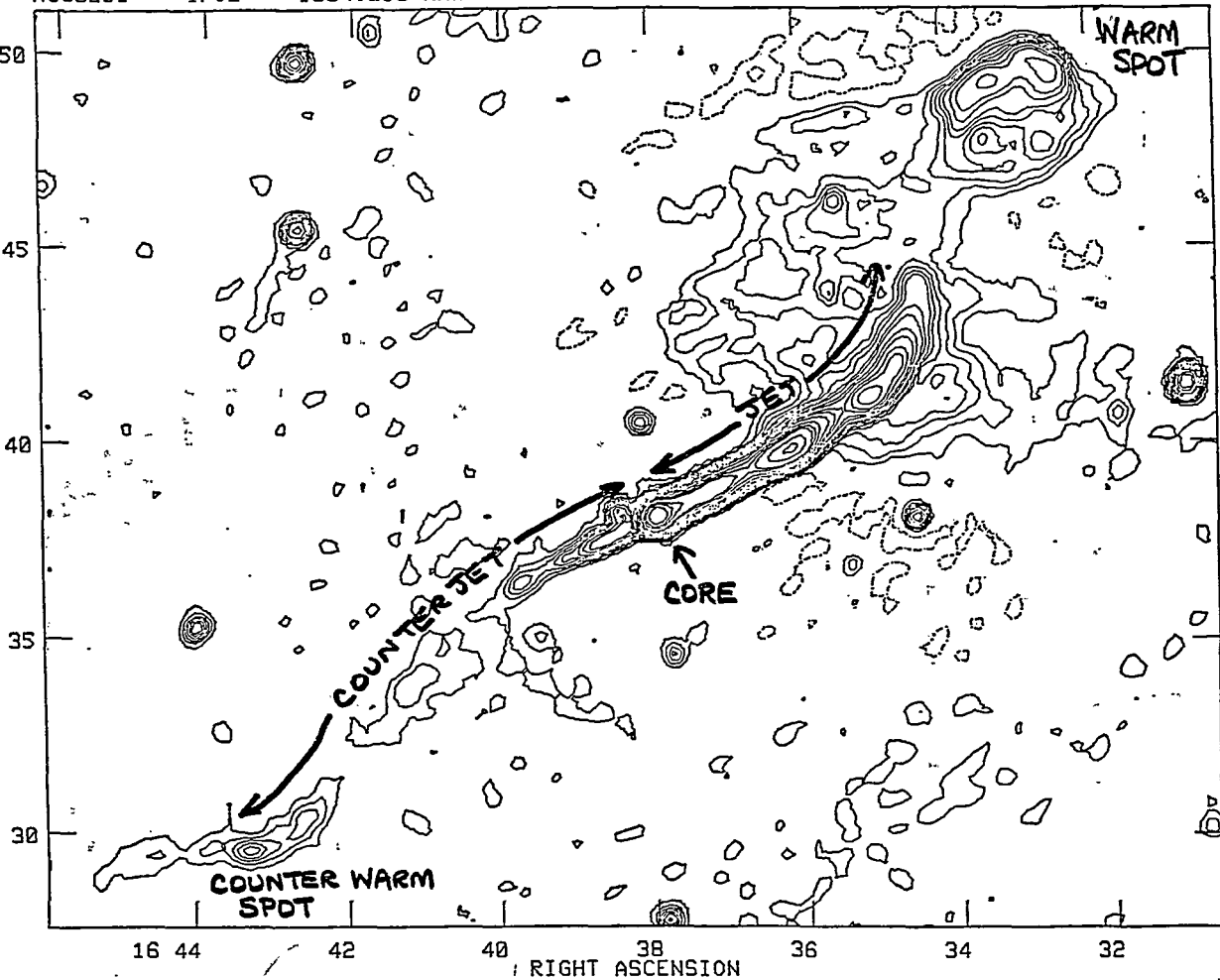


Fig. 1  
VLA 'C'  
array  
25'' resolution  
λ 18 cm

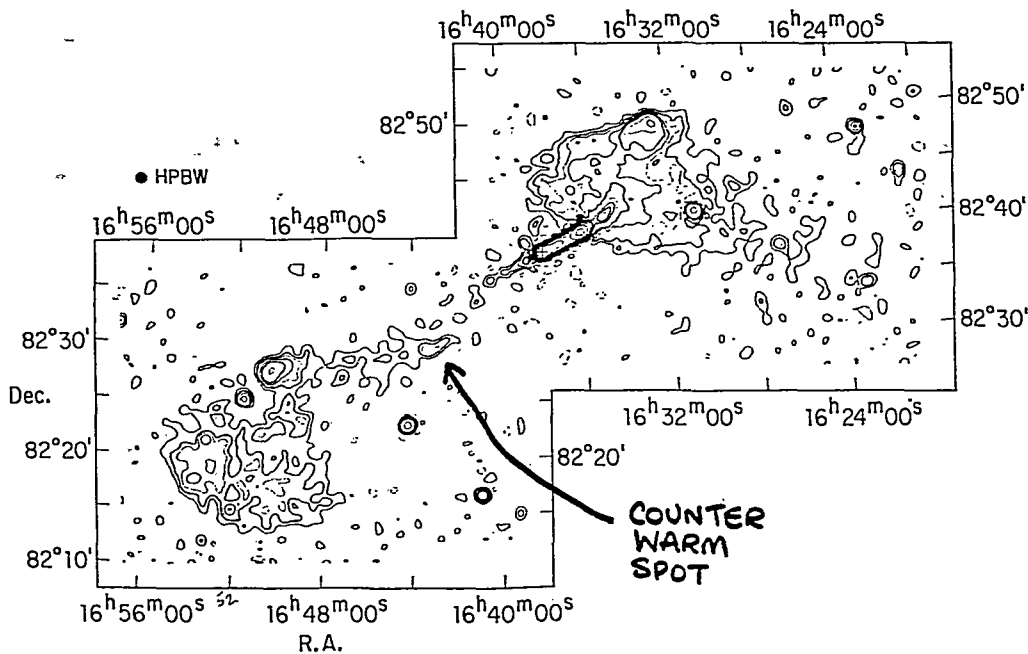


Fig. 2  
WSRT  
50'' resolution  
λ 50 cm

Fig. 1.—Map of the entire NGC 6251 source at 610 MHz with 50'' resolution (from Willis *et al.* 1982). The cross marks the position of the nucleus of NGC 6251.

TABLE 1A  
VLA OBSERVING PARAMETERS

PARAMETER	DATE			
	1979 Nov 05	1980 Mar 31	1980 Dec 05	1981 Oct 05



# ORIGINAL PROPOSAL AP66

TO: M.S. Roberts  
FROM: R.A. Perley and A.H. Bridle *Handwritten: R.A.P. and A.H.B.*  
DATE: 4 October 1982  
SUBJECT: Proposal to observe the low-brightness features of NGC6251 at 6 and 20 cm with the VLA in the C and D configurations.

We request the use of the VLA for 24 hrs in each of the C and D configurations to map total and polarized intensities of the counterjet and lobes of the large radio galaxy NGC6251. The proposal is the first of a new program intended to explore aspects of the source revealed by, or related to, our previous study of the bright jet in this object.

## BACKGROUND

NGC6251 is a 14th-magnitude elliptical galaxy with a redshift of 0.023 associated with a radio source 1.1 degrees in overall extent. For  $H=75$  km/s/Mpc the linear diameter of the source is 1.7 Mpc, making it one of the largest known radio galaxies. A high-brightness jet some 120 kpc long was discovered in the source by Waggett, Warner and Baldwin (1977). We observed this jet using the A configuration at 21 and 18cm, a hybrid (construction) configuration at 20 and 6 cm, and a D configuration "snapshot" at 20cm. The main results of these observations were:

1. Evidence that the jet may be interacting with a surrounding medium: it expands in several discrete steps, and exhibits lateral oscillations which are readily interpreted as Kelvin-Helmholtz instability modes of a confined jet.
2. Evidence that the surrounding medium may be an ionized magnetosphere of NGC6251: there are large and complex Faraday rotation gradients over the central parts of the source. These gradients cannot be due to thermal electrons and fields in the jet because there is no significant depolarization between 21cm and 6cm. Rather, the gradients, which are largest closest to the center of NGC6251, must arise in material between us and the jet but associated with NGC6251.
3. Detection in the D array snapshot of a weak counterjet whose intensity within 90" of the core is about 1/40th that of the main jet, but decreases to <1/250th that of the main jet further from the core. The reality of this counterjet is confirmed by a WSRT 610 MHz map at 50" resolution.
4. Mapping of the magnetic structure of the jet in detail: the projected field contains both parallel and perpendicular components, with deep field-parallel layers at the edges of the field-perpendicular configuration in the more expanded outer regions of the jet. There are also regions of oblique projected field which can be explained only if there are departures from axial symmetry in the internal structure of the jet.

These results will soon be submitted to the Ap.J. They raise questions about NGC6251 which we wish to explore using various combinations of frequencies and configurations, now that reduction and interpretation of the earlier data are complete. Some of the new observations require modes of operation or equipment not yet installed at the VLA; these will be requested as the VLA becomes capable of supporting them. This request is for the parts of the ongoing study which can be done now.

## STUDIES OF THE COUNTERJET

We wish to determine the internal structure, collimation and polarization

properties of the counterjet, for comparison with those of the main jet. The counterjet is too faint and resolved to be detectable at A or B configuration resolution at 20cm, but is very clear in our D configuration snapshot at this frequency (Figure 1). We require a mixture of C and D configuration observations at 20cm and 6cm to examine its structure in both total and polarized intensities. The symmetries of its expansion, brightness-width evolution, field configuration and Faraday rotation properties relative to those of the main jet are all potent tests of models for these quantities which depend on the existence of a gaseous halo around the nucleus of NGC6251. The ratio of brightnesses between the counter jet and the main jet as a function of distance from the core source is also an important constraint on theories of the jet/counterjet mechanism. We will combine C and D configuration observations of about 3 hrs duration at 21cm, 18cm and 6cm to address these matters.

## THE OUTER REGION OF THE MAIN JET

The parts of the main jet beyond about 5' from the core (see Figure 1) are resolved out in our earlier high-resolution observations but only poorly resolved in the D configuration snapshot at 20cm. Important questions about the transition between the main jet and the northwest lobe cannot be answered using the present data sets. What is the path and brightness evolution of the jet as it enters the northwest lobe? What is the magnetic structure in the region where the jet "ends", presumably sharing its momentum with the surrounding material? Can the jet be traced continuously to the "warm spot" at the northwestern edge of the source, and what is the structure of this warm spot? The latter provides an indirect constraint on the jet velocity; if the jet does reach the warm spot, it presumably has sufficient thrust to overcome the internal pressure of the spot. We therefore require maps of the northwestern lobe with better resolution than at present, but with sufficient short spacings to sample and separate structural scales from 10" to 10' (see Figure 1). We need to combine C and D configuration observations at 20cm and 6cm of at least one more phase center along the probable path of the jet in the northwestern lobe.

## ROTATION MEASURE AND SPECTRAL GRADIENTS IN THE LOBES

There is evidence from the Cambridge 151-1417 MHz observations of the lobe that the emission between the bright jet and the northwest warm spot has a spectrum similar to that of the jet, but that the more diffuse lobe emission away from the jet has a spectrum 0.5 steeper. Our data show that there is no significant spectral gradient along the jet and (from the brightness-width evolution) that particle acceleration continues for some tens of kpc along it. We wish to study both the rotation measure and spectral gradients over both lobes for comparison with the large RM gradients and negligible spectral gradients we have established for the jet. The RM data will test our interpretation of the RM gradients in the jet - we expect very little RM gradient over the lobes if the gradients over the jet indeed originate in the inner regions of a magnetosphere of NGC6251. WSRT 610 MHz data show that the lobes are significantly polarized and will be used for comparison with the VLA 20 cm observations. The C configuration observations will provide higher-resolution data for the more compact lobe features at 20cm for comparison with the VLA D configuration data at 6cm. They will also be used to measure the RMs of about five unresolved background sources which are viewed through the lobes.

The lobes of NGC6251 will also be a good arena in which to test the lobe magnetic field model of Laing (1980), wherein the field is sheared so as to be tangential to the surface of the lobe, with no radial component, but is otherwise random. To test this model quantitatively, we need to establish the projected

magnetic field direction over the lobe, and to check for depolarization over it. Previous tests of the model in M84 (Laing and Bridle, in preparation) met with different degrees of success on the two different sides of the same source; again in the presence of large-scale RM gradients believed to be associated with the parent object. NGC6251 is suitable for further tests of the Laing model, as its lobes are bright, two-dimensional structures over which the VLA can map many pixels. To determine polarization structure (with typical degrees of polarization of 20%), 1-hr integrations at 50 MHz bandwidth are required for several phase centers at 20cm. Due to the 1.1 degree size of the source, three separate phase centers are required for the northwest lobe, counterjet, and southeast lobe observations, even at 20cm.

#### TIME REQUEST

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We request 24 hrs in each of the D and C configurations of the VLA for these observations. In the D configuration, we will spend about 1 hr at each of three phase centres at 20cm, and the balance of the time at 6cm. We will be able to specify the time and frequency distribution of the C configuration observations in detail only after the D configuration data are available, but presently estimate our requirement as 24 hrs mainly at 20cm. Due to the 83 degree declination of NGC6251, a single 24-hr run in each configuration is feasible.

#### REFERENCES

Laing, R.A. 1980. M.N., 193, 439.  
Waggett, P.C, Warner, P.J., Baldwin, J.E. 1977. M.N., 181, 465.

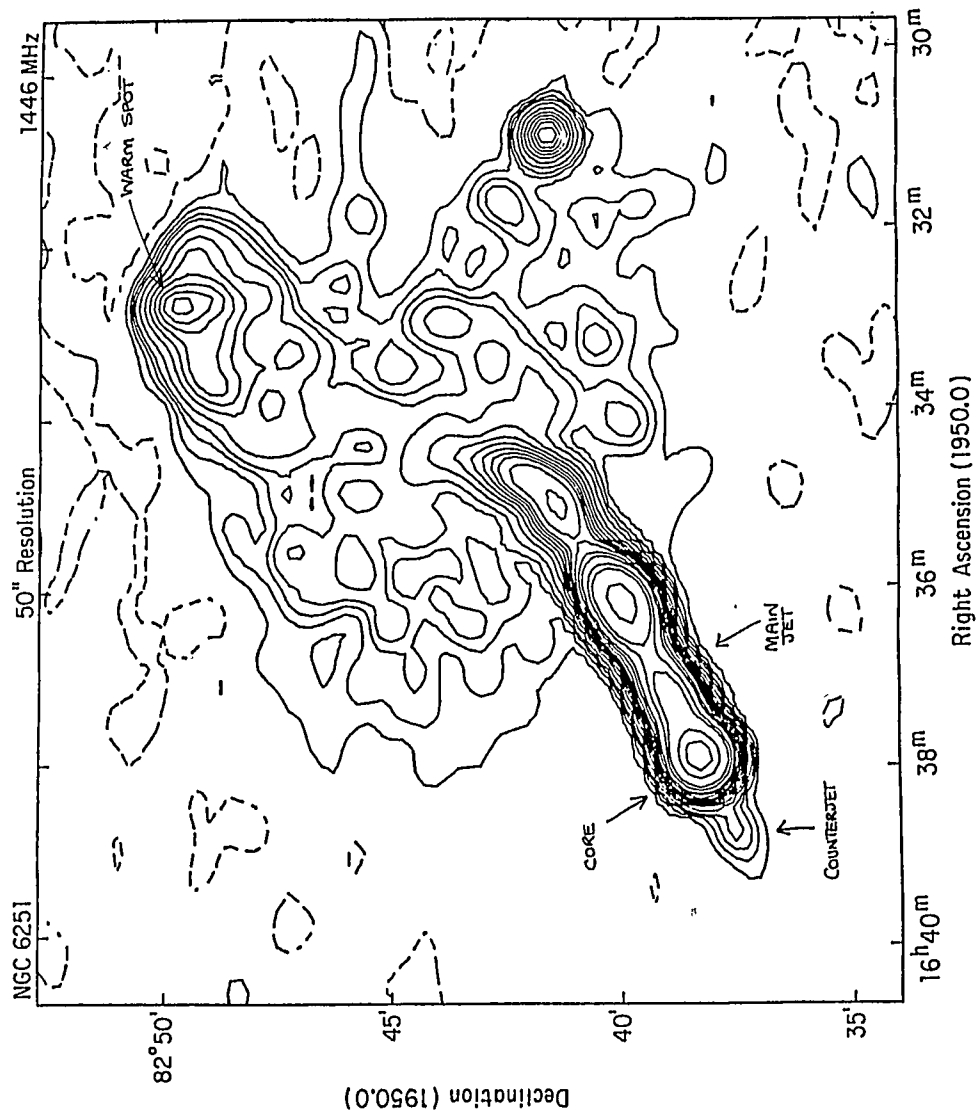


Figure 1

From: VAX3::RICK 12-JUN-1983 16:00  
To: CVAX::BRIDLE  
Subj: chagrin, embarassment, shame

I have just scanned our run from last night, and discovered the observe file had a crucial error. The A/C Fluke setting was 12.5 MHz too high, causing the 50MHz passband to contain only 37.5MHz width of data. Fortunately, this only occurred on the calibrator 1803+784. All the observations of NGC6251 are all right, as are the observations of 3C48 and 3C138. It appears that only polarization calibration will suffer, and we'll probably be able to recover that from next week's run.

I cannot explain how this happened. I used SOS to substitute 100.0 and 200.0 (the correct settings) for 112.5 and 212.5 (the old setting used for the C array data). All the 212.5 did change to 200.0 (hence, the B/C

oops, I mean B/D data are o.k.), however, only the 112.5 Fluke settings on cards of the source, 3C48, and 3C138 changed. Somehow, I goofed. Of course, the real error was in the lack of adequate final checking, and for that I am truly sorry. I just hope we can recover the polarization calibration next week.

The operator said he saw no interference. I won't know for sure until tomorrow. I'll make a quick map, and let you know.

From: VAX3::RICK 11-JUN-1983 15:21  
To: CVAX::BRIDLE  
Subj: New observations

I used my two hours of test time to integrate on the following frequencies: 4885, 4835, 1665, 1515, 1485, and 1435MHz. All were pretty clean except 1435 MHz, which had a lot of sporadic RFI, and one scan which was completely blown away. Thus, I believe we should do the following for tonight:

- 1) Observe the core at 4885/4835 MHz. No problem here.
- 2) Observe near the warm spot for 1 hour.
- 3) Observe the core at 1665/1515 MHz.
- 4) Observe the S lobe at 1465/1515 MHz.

In all cases, the more important/more reliable frequency is in the A-C channels. I thought that 2 hours on the core at 6cm, and 1.5 hours at each of the 20cm pairs (S lobe and core) plus the 1 hour at the warm spot should do.

I have been mulling over your comment about deferring the 6cm observations. Sounds good to me from an interference point of view. This (meaning tonight) is a night/weekend run, and much less likely to be zapped

Cancel the above argument which I didn't finish. The long run next week is a midnight run. Nevertheless, given the reliability of the 6cm observations, it makes good sense to test the waters at 20cm now, on a weekend. I'll make up the file at 20cm only, using items 3 and 4 above. I'll split the time equally between the two observations. Any comments?

From: VAX3::RICK  
To: CVAX::BRIDLE  
Subj: New observation

11-JUN-1983 10:04

O.K. I'm at the site. It turns out that I have test time starting in one hour. I plan to tune to these new frequencies, and integrate for a while. Of course, I'll use NGC6251 as the object to integrate upon. The bug in filler which was ruining all the 4-IF data has now been repaired (turned out that the signs of the real and imaginary parts were being reversed), so I can properly calibrate the 2 hours of test data I took on blank sky a couple nights ago. This will tell us the best (i.e. least noisy) frequencies. I'll select the best (subject to careful reading of your comments from yesterday), and integrate on them for a while, to see if occasion RFI lurks about.

More late. Call the operator to get me.

From: VAX3::RICK 9-JUN-1983 10:13  
To: CVAX::BRIDLE  
Subj: New obs, and B/D IFs.

The B/D ifs are here, and they seem to operate. I ran a few hours of tests to find optimal frequencies. The best contiguous frequencies are 1465 and 1515 MHz. An alternative good pair are 1435 and 1485MHz. These have the advantage of averaging close to 1465MHz, the old default frequency. We're observing on Sunday, so we need to consider which pairs we would like. At 6cm, virtually any frequency can be chosen. 4885 and 4835MHz seem to work well.

If, on the other hand, we choose to spread our L-band frequencies, I got good results on any frequency except those which overlap 1600MHz (an enormous internal birdie). I am not in favor of this, however, as we have previously selected (for C array) 'median' frequencies. Furthermore, the noise noticeably increases below 1400MHz. So, I think either 1465/1515 or 1435/1485 are the best bets. Any preferences? Note that the B/Ds seem to work, but there are a few bugs left, such as bad samplers, which seem to cause high closure errors on a few correlators. The situation is similar to the A/C situation a few years ago.

There is a serious bug either in Filler or Antsol which is causing amazing errors in Antsol listings. I am convinced, however, that it is a software problem, and not due to the 4 IFs per se. The data looks good.

As part of the Baars et al experiment that Pat Crane and I are taking care of (checking the Baars flux scale), we have gotten a fair amount of data on 3C274. My summer student arrived yesterday, and I decided to use this data to cut his teeth on the VAX. We got an impressive map of the halo. The remarkable thing is the evidence for rotation of the jet as a function of scale size. I'll send a copy of the map over the wire to you.

How's the review coming? Haven't heard from you in a few days.

For the S lobe, we used 1452.4

jer

1664.25

From: VAX3::RICK  
To: CVAX::BRIDLE  
Subj: RE: Misc. matters

12-APR-1983 18:04

The VLbers do phase the A and C if-s independently, but so long as they use the same antenna for both, and the true A-C phase of that antenna doesn't change, there should be no problem. The potential problem is that the stupid VLB program may take a different reference antenna each time it phases up. It has some criterion by which it decides which antenna is best, and this criterion or criteria does not account for phase jumps. If there were no phase jumps in any antenna, then changing the reference antenna won't hurt the polarization. The danger is in the phase jumps, and as we all know, phase jumps are rather common here. I don't believe there is any record of which antenna was taken as reference, and of course you know that most phase jumps are invisible to the monitoring system. By the way, self-cal also adjust A and C IFs independently, with no deleterious result to polarization.

The only way I can think of to check the behaviour is to list the AC phases for 1803+784. Pat put in three observations of this source for every observation of NGC6251. Fortunately, 1803+784 has quite a respectable polarization. We should be able to learn a lot from this. Keep your fingers crossed.

To bad about the glossies. Will bribes help? Interesting info about Jennison.

From: VAX3::RICK 11-APR-1983 15:11  
To: CVAX::BRIDLE  
Subj: More N6251 Observations

Barry has tentatively scheduled our D-array N6251 observations for Sunday, June 19. Are you able to come for these observations, too? Given that we all leave for Italy shortly afterward, it seems reasonable to assume that you won't be able to come. I think it is also reasonable to presume that at that time I'll be frantically working to complete my talk! I notice that you're not listed to give a talk at Bologna. Want some compact source data? Blowing hard today. New storm coming in.



# Jet Velocity estimates in NGC6251

March 1983

## (a) Steady-State Energy Balance

$$F = (U_{int} + \frac{1}{2} \rho_j v_j^2) v_j \cdot \pi R_j^2 = L_{lobe} / \Sigma$$

$$L \sim 10^{24} \text{ @ } 1480 \rightarrow$$

$$L_{lobe} = 1.1 \times 10^{32} (v_{max}(\text{Hz}))^{0.3} \text{ wcts}$$

$$v_{max} = 10 \text{ GHz}$$

$$L_{lobe} \sim 10^{24} \text{ W/Hz/ster at } 1480 \text{ MHz} \rightarrow 1.1 \times 10^{35} \text{ Wcts.}$$

$$\theta = 227''$$

$$\Delta R M < S \rightarrow n_e < 2 \times 10^{-4} \text{ cm}^{-3} \equiv 200 \text{ m}^{-3}$$

$$\rho_j < 3.35 \times 10^{-31} \text{ kg/cm}^3 \equiv 3.35 \times 10^{-25} \text{ kg/m}^3$$

$$U_{min} \sim 6 \times 10^{-13} \text{ J/m}^3$$

$$U_{min}/c^2 \sim 6.68 \times 10^{-30} \text{ kg/m}^3$$

$$R_j \sim 6'' \cdot 5 \sim 2.8 \text{ kpc} \sim 8.6 \times 10^{19} \text{ m}$$

$$A = \pi R_j^2 = 2.35 \times 10^{40} \text{ m}^2$$

$$\text{Hence: } (6 \times 10^{-13} + \frac{1}{2} \times 3.35 \times 10^{-25} v_j^2) v_j \cdot 2.35 \times 10^{40} = \frac{1.1 \times 10^{35}}{\Sigma}$$

$$1.28 \times 10^{-7} v_j + 3.59 \times 10^{-20} v_j^3 = 1/\Sigma$$

If:	$\Sigma = 1$	0.1	0.05	0.04	0.03	0.01	
$v_j =$	2640	6350	8080	8730	9630	14000	km/s

light jet  $\frac{1}{2} \rho_j v_j^2 \ll U_{min} \quad v_j \rightarrow \frac{7801}{\Sigma} \text{ km/s}$

Heavy jet  $\frac{1}{2} \rho_j v_j^2 \gg U_{min} \quad v_j \rightarrow \frac{3031}{\sqrt[3]{\Sigma}} \cdot \left( \frac{3.4 \times 10^{-25}}{\rho_j (227'')} \right)^{1/3} \text{ km/s}$

$$\theta = 32''$$

Depol  $\rightarrow$

$$n_e < 4 \times 10^{-3} \text{ cm}^{-3}$$

$$\rho_j < 6.7 \times 10^{-30} \text{ kg/cm}^3 \equiv 6.7 \times 10^{-24} \text{ kg/m}^3$$

$$u_{\text{min}} \sim 5.4 \times 10^{-12} \text{ J/m}^3$$

$$R_j \sim 1''.75, 0.75 \text{ kpc} \sim 2.31 \times 10^{19} \text{ m}$$

$$A = \pi R_j^2 = 1.69 \times 10^{39} \text{ m}^2$$

$$\text{Hence } (5.4 \times 10^{-12} + \frac{1}{2} \times 6.7 \times 10^{-24} v_j^2) v_j \cdot 1.69 \times 10^{39} = \frac{1.1 \times 10^{35}}{\epsilon}$$

$$8.28 \times 10^{-8} v_j + 5.14 \times 10^{-20} v_j^3 = \frac{1}{\epsilon}$$

If $\epsilon =$	1.0	0.1	0.04	0.01	
$v_j =$	2490	5710	7,800	12,400	km/s

$$\text{light jet } v_j < \frac{12000}{\epsilon} \text{ km/s}$$

$$\text{Heavy jet } v_j \approx \frac{2690}{\sqrt[3]{\epsilon}} \left( \frac{6.7 \times 10^{-24}}{\rho_j} \right)^{1/3} \text{ km/s}$$

Suppose we accept expansion rate velocity  $v_j \sim 8000 \text{ km/s}$

$$\epsilon \sim 0.04$$

$$\rho_j \sim 6.7 \times 10^{-24} \text{ @ } \theta = 32''$$

$$\left. \begin{aligned} \frac{1}{2} \rho_j v_j^2 &= 2.14 \times 10^{-10} \text{ J/m}^3 \\ u_{\text{min}} &= 5.4 \times 10^{-12} \text{ J/m}^3 \end{aligned} \right\} \underline{\underline{39.7:1}}$$

Method (b). Expansion rate.



$$\tan \alpha = \frac{v_r}{v_j \cos i} \\ = \frac{c_s}{M c_s \cos i}$$

If the jet is "free" at  $(h) \leq 17''$ ,  $M \sim 14^{\text{seci}}$  there.  $M = \cot \alpha \sec i$

At  $(h) = 17''$ , from BCH fit,  $\frac{f_{17}}{f_{32}} = \frac{0.25}{0.32} = 0.78$   $f_{17} = 5.2 \times 10^{-24} \text{ kg/m}^3$

From equipartition  $(h) = 17''$   $u_{\text{min}} = 4.4 \times 10^{-12} \text{ J/m}^3$ .

$$p_{\text{min}} (\text{using } \times 0.86 \text{ factor}) \rightarrow 1.26 \times 10^{-12}$$

$$\text{Then } c_s = \sqrt{\frac{\partial p}{\partial \rho}} = \sqrt{\frac{1.333 \times 1.26 \times 10^{-12}}{5.2 \times 10^{-24}}} = 5.68 \times 10^5 \text{ m/s}$$

$$\text{Hence } v_j = M c_s = 14 \times 5.68 \times 10^5 \text{ seci} \rightarrow 7.95 \times 10^6 \text{ m/s seci} \\ \rightarrow \underline{\underline{8000 \text{ km/s. seci}}}$$

NB BCH fit itself  $\rightarrow M \approx 5.4$

$$v_j = \underline{\underline{3000 \text{ km/s.}}}$$



Method (c). Thrust balance

Warm spot in 50" 1446 MHz snepnep

- peak I = 33.3 mJy

$$\theta_{\text{obs}} = 1.8 \approx 108''$$

$$\theta = \sqrt{108^2 - 50^2} = 96'' \text{ intrinsic}$$

$$R_{\text{HS}} = 48'' \rightarrow 20.6 \text{ kpc} = 6.35 \times 10^{20} \text{ m}$$

Assume 0.7 index  $\nu \sim 1 \text{ MHz} \rightarrow 1 \text{ GHz}$  (same  $E_{\text{range}}$  as jet) <sup>177 MeV lowest</sup>

$$B_{\text{eq}} \sim 2.6 \times 10^{-6}$$

$$u_{\text{min}} \sim 6.18 \times 10^{-14}$$

$$p_{\text{HS}} A_{\text{HS}} = \frac{0.86 \times 6.18 \times 10^{-14} \times \pi \times (6.35 \times 10^{20})^2}{3}$$

$$= 2.24 \times 10^{28} \text{ Nt.}$$

Momentum flux delivered to lobe is  $f_j \rho_j^2 v_j^2 \cdot A_j$   $f = \frac{1}{1 + \sqrt{\beta_j/\beta_{\text{rem}}}}$

$$\text{(i) } = 227'' \text{ parameters } \left. \begin{array}{l} f_j = 3.35 \times 10^{-25} \\ A_j = 2.35 \times 10^{40} \end{array} \right\} v_j = 1.69 \times 10^6 \left( \frac{3.35 \times 10^{-25}}{f_j} \right)^{1/2} \cdot \frac{1}{f}$$

$$\text{(ii) } = 32'' \left. \begin{array}{l} f_j = 6.7 \times 10^{-24} \\ A_j = 1.69 \times 10^{39} \end{array} \right\} v_j = 1.41 \times 10^6 \left( \frac{6.7 \times 10^{-24}}{f_j} \right)^{1/2} \cdot \frac{1}{f}$$

So for  $v_j = 8000 \text{ km/s}$ , need  $f \sim 0.194$   $f_j \sim 17 \text{ SIGM}$  at hotspot.

Problem  $\rho v R^2$

Method (d)

If it's heavy  $\frac{1}{2} \rho_j v_j^3 A_j = \frac{L_{\text{lobe}}}{\Sigma}$  for energy balance

$$\rho_j \xi^2 v_j^2 A_j = \rho_{\text{HS}} A_{\text{HS}} \quad \xi = \frac{1}{\sqrt{1 + \sqrt{\rho_j / \rho_{\text{HS}}}}}$$

$$v_j = \frac{2 L_{\text{lobe}} \xi^2}{\rho_{\text{HS}} A_{\text{HS}} \Sigma}$$

$$= \frac{2 \times 1.1 \times 10^{35} \xi^2}{2.24 \times 10^{28} \Sigma}$$

$$\lesssim \frac{9820 \xi^2}{\Sigma} \text{ km/s.}$$

# NGC6251 outflow argument

$$V_j^3 > \frac{2L_{\text{lobe}} d_{\text{HS}}}{\Sigma M_{\text{bit}}}$$

$$1 \text{ yr} = 3.156 \times 10^7 \text{ sec}$$

For Mbar, take Faber/Gallagher (ApJ, 204, 365 (1976))

$$\text{Gas ejection rate from old stars in E galaxy} = 0.015 M_{\odot}/\text{yr} / (10^9 L_{\odot})$$

Absolute magnitude of NGC6251:  $M_{\text{BCO}} = -21.3$   $\frac{1.2 \times 10^{12} M_{\odot}}{+5.48}$

Sun

Hence ~~26.8~~  $26.8 = 2.5 \log(L/L_{\odot}) \rightarrow 5 \times 10^{10} L_{\odot}$

$$\rightarrow \sim 0.8 M_{\odot}/\text{yr}$$

$M=75 \rightarrow \tau_{\text{H}} \sim 1.3 \times 10^{10} \text{ yrs} \rightarrow 10^{10} M_{\odot}$  available  $\sim 10^{-2}$  galaxy?

$$L_{\text{lobe}} = 1.1 \times 10^{35} \text{ Watts}$$

$$d_{\text{HS}} = 16'' = 960'' = 212 \text{ kpc} = 1.27 \times 10^{22} \text{ m}$$

$$V_j^3 > \frac{1.1 \times 10^{35} \times 1.27 \times 10^{22} \times 2}{\Sigma \times \frac{1}{2} \times 10^{10} \times 1.585 \times 10^{30}}$$

$$= \frac{1.41 \times 10^{57}}{\Sigma}$$

$$V_j = 5.2 \times 10^5 / \sqrt{3 \Sigma} \text{ m/s}$$

$$= \frac{656}{\sqrt{3 \Sigma}} \text{ km/s}$$

For  $\Sigma = 0.04$ , this gives  $V_j > 1640 \text{ km/s}$   $V_j \sim 800$   $\tau \sim 6 \times 10^7 \text{ yrs}$

$$\tau > 3.1 \times 10^8 \text{ yrs}$$

$$dM/dt \lesssim 320 M_{\odot}/\text{yr} \text{ (hot jets)}$$

Note, could have taken other lobe,  $d = 38'' \rightarrow V_j > \sqrt{\frac{38}{16}} \times 520 / \sqrt{3 \Sigma}$

$$\rightarrow 694 / \sqrt{3 \Sigma} \text{ km/s}$$

What's the optimum set of parameters for heavy N62S1?

We have various estimates:

1) Energy balance  $v_j = \frac{2690}{\sqrt[3]{\epsilon}} \left( \frac{6.7 \times 10^{-24}}{f(32'')} \right)^{1/3}$  km/s  
① = 32''

2) ~~Thrust~~ Thrust  $v_j = \frac{1400}{f} \left( \frac{6.7 \times 10^{-24}}{f(32'')} \right)^{1/2}$  km/s

3) Expansion  $v_j = 8000 \text{ sec}(i) \left( \frac{6.7 \times 10^{-24}}{f(32'')} \right)^{1/2}$  km/s

4) Mass Flow  $v_j \geq \frac{520}{\sqrt[3]{\epsilon \epsilon_0}} \left( \frac{5 \times 10^9 M_\odot}{M_{\text{tot}}} \right)^{1/3}$  km/s

To balance energy and thrust we need  $\frac{2690}{\sqrt[3]{\epsilon}} \sim \frac{1400}{f}$  roughly  
 $f^3 \sim 0.14 \epsilon$ .

So even for  $\epsilon = 1$ ,  $f$  must be  $\leq 0.52$

This requires  $f_{\text{jet}} \gtrsim 0.9 f_{\text{EM}}$ .



To balance thrust and expansion we need

$$8000 \text{ sec}(i) = \frac{1400}{\eta}$$

$$\underline{\underline{\eta = 0.18 \text{ sec}(i)}}$$

This is much harder, and requires  $\eta < 0.18$

$$\text{i.e. } \beta_j > 20 \times \beta_{\text{ISM}} !!$$

This is a big problem. It means we must have underestimated  $p_{\text{HS}}/k_{\text{HS}}$  somehow, if it's in pressure equilibrium. Either the hot spot is far from equipartition, or we have got very bad parameters for it.

As  $v_j \sim \sqrt{p_{\text{HS}}}$ , increasing  $v_j$  by a factor 57 corresponds to increasing  $p_{\text{HS}}$  by a factor  $\sim 33$ . This hot spot is  $\sim 1/33$  the pressure we would have expected. To balance energy budget and expansion

$$\frac{2690}{\sqrt[3]{\epsilon}} \sim 8000 \text{ sec } i$$

$$\underline{\underline{\epsilon \sim 0.04 \text{ sec}^3 i}}$$

$$\cos^2 i \text{ @ } 10^\circ = 0.96$$

$$20^\circ \quad 0.83$$

This is the constraint we had in the draft paper, with  ~~$\epsilon$~~   $i = 0^\circ$ .

Putting this in mass flow,

$$\frac{\cancel{360} 656}{0.34 \text{ sec } i \sqrt[3]{\epsilon_0}} \left( \frac{5 \times 10^9 M_\odot}{M_{\text{tot}}} \right)^{1/3} = \frac{8000}{\cos i}$$

$$(0.24)^3 = \frac{1.4 \times 10^{-2}}{\cancel{3.0 \times 10^{-2}}} = \frac{\epsilon_0 M_{\text{tot}}}{5 \times 10^9 M_\odot}$$



So  $\boxed{7.0 \times 10^7 M_{\odot} = \Sigma_0 M_{\text{tot.}}$  - minimum ejected mass.

$\Sigma_0 \sim 0.1 ?$

$M_{\text{tot}} \sim 4.5 \times 10^8 M_{\odot}$  - fuel available.

Things would be much simpler if we had a value for  $p_{\text{HS}} A_{\text{HS}}$  that was  $\sim 25 \times$  greater.

or if the jet had been decelerated? by a factor of five between the  $\odot \sim 227''$  region and the hot spot.

So if the scale is  $\sim$  correct, need  $f^{4/7} \sim (1/25)$   
 $f \sim 0.0036 !$

i.e. there has to be something much smaller out there containing most of the flux?

Suppose we let  $v_j = 8000 \text{ km/s}$   
 $\xi = 0.04$

$$\begin{aligned} \text{At } \textcircled{H} = 32'' \quad \frac{dm}{dt} &= \int_j v_j A_j = 6.7 \times 10^{-24} \times 8 \times 10^6 \times 1.69 \times 10^{39} \\ &= 9.06 \times 10^{22} \text{ kg/s} \\ &= 1.44 M_{\odot}/\text{yr} \end{aligned}$$

$$\left( 1 M_{\odot}/\text{yr} = \frac{1.989 \times 10^{30} \text{ kg}}{3.156 \times 10^7 \text{ sec}} = 6.30 \times 10^{22} \text{ kg/s} \right)$$

$$\textcircled{H} = 227''$$

$$\begin{aligned} &= 3.35 \times 10^{-25} \times 8 \times 10^6 \times 2.35 \times 10^{40} \\ &= 1.00 M_{\odot}/\text{yr}. \end{aligned}$$

Suppose we set

$$\cancel{\rho_{HS}} \rho_{IEM} v_{HS}^2 \sim p_{HS}$$

$$\rho_{IEM} \sim 10^{-26} \text{ kg/m}^3$$

$$p_{HS} \sim \frac{0.86 \times 6.18 \times 10^{-14}}{3} = 1.77 \times 10^{-14}$$

$$\text{then } v_{HS}^2 = 1.8 \times 10^{12}$$

$$v_{HS} = 1.3 \times 10^6, \text{ or } 1300 \text{ km/s.}$$

So there is no difficulty providing ram pressure for confinement at this density.

## Synchrotron scales.

Inner jet  $B \sim 25 \mu\text{gauss}$   $5\text{GHz} \rightarrow 3.5 \times 10^9 \text{eV}$   $\tau_{\text{synch}} \sim 3.79 \times 10^6 \text{yrs.}$

At  $8000 \text{ km/s}$ ,  $\tau_{\text{synch}}$  is  $9.57 \times 10^{20} \text{ metres}$   
 $\sim 3.1 \times 10^4 \text{ pc} = 31 \text{ kpc} = \underline{\underline{72''}}$

Outer jet  $B \sim 7 \mu\text{gauss}$   $5\text{GHz}$   $\tau_{\text{synch}} \sim 2.56 \times 10^7 \text{ yrs.}$   
At  $8000 \text{ km/s}$ ,  $\rightarrow 6.46 \times 10^{21} \text{ metres}$   
 $\rightarrow 2.1 \times 10^5 \text{ pc}$   
 $\rightarrow 488''.$

Therefore not surprising that we see no spectral gradients, as even if all  $5\text{GHz}$  particles had been generated at  $\sim 10''$ , we could transport them out at  $8000 \text{ km/s}$  slightly faster than we age them due to synchrotron losses.



## Deflection of NGC6251 jet.

What angle does it deflect through?

Radius of curvature from the WRT map is  $\sim 10' \sim 600''$   
 $\sim 257 \text{ kpc}$

$$r_c = 257 \times 3.08 \times 10^{19} \text{ m.}$$

$$v_j = \left( \sqrt{\frac{\rho_{\text{ISM}} r_c}{\rho_j h}} \right) v_g$$

Inside the 30 kpc scale ISM  $r_c = \text{large!}$  (jet straight)

Outside,  $h \sim d_{\text{jet}} \sim 16''$

$$v_j = v_g \sqrt{\frac{\rho_{\text{ISM}}}{\rho_j} \cdot \frac{600}{16}} \sim 6 v_g \sqrt{\frac{\rho_{\text{ISM}}}{\rho_j}}$$

Using our estimates, we have  $\rho_{\text{ISM}}/\rho_j \sim 3?$

$$\underline{v_j \sim 10 v_g}$$

Don't know  $v_g$ , but unlikely to be  $\gg 1000 \text{ km} \cdot \text{s}^{-1}$

$$\underline{v_j \sim 10,000?}$$

If we used  $h \sim \text{jet diameter}$  or hor spur  $h = \underline{96''}$

$$v_j = v_g \sqrt{\frac{\rho_{\text{ISM}}}{\rho_j} \cdot \frac{600}{96}} = 2.5 \sqrt{\frac{\rho_{\text{ISM}}}{\rho_j}} v_g$$

4 100 0 0

Re your comments on the power spectra:

Indeed the angle data generally give better spectra (in terms of significant peaks) than the deflection data. This is an important point, as it means that the deflections ARE growing with distance from the core, in general.

When estimating significance, it is important to compare spectra at the same resolution. The only spectra whose significance should be judged from the Gaussian-noise spectrum at the front of the ones I sent you are the 256-resolution spectra. The reason why the 0.19 r.u. peak in the first spectrum looked puny is because that was a 128-resolution spectrum. It looks o.k. compared with the noise spectrum at its resolution (which, of course, I didn't send you !).

I don't know what to make of the broader peaks. They usually resolve at higher resolution into numbers of smaller peaks. I tend to think we should look at the peak excursions from the LOCAL MEAN LEVEL in the power spectrum, in which case these broad peaks are not as significant. Certainly they correspond to "things" in the spectra, whether real oscillations or not, which are not simple harmonic in the way that naive Kelvin-Helmholtz modes would be. I have therefore focused more on the "sharp" peaks so far.

The coming and going of peaks as we vary the distance range is not surprising - I could pick some small distance ranges out of the data and really blow up individual spectral peaks - e.g. the 31" oscillation at the beginning of the "outer" jet. In general I feel happier about spectra which exclude the angle data from the first 10" or so from the core, where we have those very rapid oscillations that decay away. These are obtained by dividing very small deviations by very small distances, and I am suspicious about their reality. Pity we can't carry the errors in individual points through the power spectrum analysis. I do feel the spectra with the close-in angle data excluded are more trustworthy, though.

The "averaged angle" plots are from data where I first plotted all of our results at different resolutions on the same scale (as in the Figures for the paper), then drew an "average" curve through by eye. That curve was then read off every 2" along the jet to get the data whose power spectra were shown. This is o.k. over a limited range of distances from the core - otherwise the effective resolution of the data varies somewhat even though its angular spacing doesn't.

I'll do some more quantitative things regarding statistical significance, then get back to you with revised text and some more power spectrum examples.

I'm starting to revise the Discussion section now. One of the first things I looked at is whether the Chan-Henriksen model we fitted should in fact have "detached" from the confining pressure according to Bob Sanders' criterion. According to his power-law expression it should have done, but according to the detailed criterion (local expansion velocity becoming locally supersonic) it shouldn't. I think the difference lies in the fact that his criterion as given in his paper is in fact only ASYMPTOTICALLY correct. In the 'real' jet, the external pressure changes before the jet has had TIME (distance from the core) enough to detach. I am therefore happier about our use of the CH model than I was when I talked to you from Queen's, but will look into this some more. What is clear is that if the nozzle was somewhat lower than we have modelled it, the jet might have detached sooner and thereby set up the situation where it became free by the

time we hit it with the "halo" pressure - generating the reconfinement shocks that Bob's paper was basically about. More to follow as I think it through and do a small number of further sums.

I got a letter from Jean-Luc Nieto with preprints of his NGC6251 paper, which has been rejected once. His pictures certainly don't show very much in the form he sent them to me, but he says he has some more observing time coming up soon, and we will keep in contact.

More ski holidays, eh ? Enjoy it while you can !

From: VAX3::RICK  
To: CVAX::BRIDLE  
Subj: n6251

3-FEB-1983 16:00

I have received your message, and am about to print the new version. I have looked over the deflection spectra and must confess that I'm a little worried about the changes in the significance of the peaks. For example, in the second plot (1.3" data, all distances), do we consider the broad peaks at 0.33 and 0.45 reciprocal units significant? They (especially the former) are almost as significant as the marked peak at 0.19 units (5.8"). Furthermo comparing to the Gaussian noise plot above, none of the peaks seems big enoug Use of 256 resolution does seem to help, though as the next plot (#3) does seem to enhance the "proper" peak at 0.19 r.u. (reciprocal units). Looking through the remaining plots, I notice that the last three (all at 2" separation) show interesting differences. The second of these shows a semi-significant peak at 0.32 r.u. This peak also shows up in the first of these three plots, although at a lower level. However, the last of these plots has no trace of said peak - in fact, there's an enormously deep trough! It seems that restriction of the range has made a great difference. This last plot is by far the most convincing in terms of the significance of the various peaks we have previously identified. By "averaged angle", do you mean that the points are averages of nearby measured values?

It seems to me that the angle data gives a better spectrum than the deflection data.



Some further power spectrum thoughts -

I tried a set of different Gaussian random number streams, each 100 points long, with the power spectrum analysis program at 256 resolution. All of them gave basically similar "phoney peak" statistics. Features of width several channels and peak amplitude five or more times the average of surrounding channels cropped up about five times per spectrum. Similar features with peak amplitude seven or more times the average of surrounding channels cropped up once per spectrum. We could therefore be pretty sure of anything that was as much as eight or nine times the surroundings, very sure of anything ten times the surroundings. I'll go through my individual 6251 spectra now and see which ones survive the test.

They're forecasting snow here now. We shall see.

# TEST

Book No. \_\_\_\_\_ of \_\_\_\_\_ Books

(SURNAME FIRST)

Section \_\_\_\_\_

NGC 6251 X-ray luminosity [from Bill Ku's 22,000<sup>s</sup> of Einstein IPC data]

$$z = 0.023, H_0 = 75 \text{ km/s/Mpc} \rightarrow D = 92.4 \text{ Mpc} = 92.4 \times 10^6 \times 3.0856 \times 10^{18} \text{ cm} \\ = 2.853 \times 10^{26} \text{ cm}$$

"Nuclear" X-ray source is  $1.4 \times 10^{-12} \text{ erg/cm}^2/\text{sec}$  [0.5-4.5 keV] - IPC.

$$L_x = 1.4 \times 10^{-12} \times 4\pi \times [2.853 \times 10^{26}]^2 \\ = 1.4 \times 10^{42} \text{ erg/s.}$$

Halo is  $\lesssim 15\%$  =  $2.1 \times 10^{41} \text{ erg/s.}$  ( $\sim 5'$  radius), i.e.  $\sim 154 \text{ kpc}$  radius.

Minimum jet pressure =  $0.86 p_{eq}$ , hence  $n_{min} = 0.86 n_{eq}$  for confinement, given  $T$   
 $L_{min} = 0.74 L_{eq}$  - - - - -

Taking our old "halo" values  $T = 4 \times 10^7 \text{ K}$   
 $L_x$  was  $2.0 \times 10^{42} \rightarrow \underline{1.5 \times 10^{42} \text{ erg/s.}}$   
within 50 kpc (116")

Angular resolution of IPC is: 95" for 0.5-4.5 keV, i.e. 42 kpc.

Hence their "nuclear source" is our core + some halo.

Q. How much of our halo is well inside IPC "beam" ?

of M87  $\sim 1.5 \times 10^{43} \text{ erg/sec}$

## Table 4

0.5-4keV luminosity and mass of media  
required to confine NGC6251 jet

Assumed isothermal temperature

		$4 \times 10^7 \text{ K}$	$2 \times 10^7 \text{ K}$	$10^7 \text{ K}$	
"HALO"	Lx	$2.0 \times 10^{42}$	$6.7 \times 10^{42}$	$1.6 \times 10^{43}$	erg/s
	M	$1.8 \times 10^{11}$	$3.6 \times 10^{11}$	$7.1 \times 10^{11}$	$M_{\odot}$
"CORE"	Lx	$7.0 \times 10^{43}$	$2.3 \times 10^{44}$	$5.6 \times 10^{44}$	erg/s
	M	$1.9 \times 10^9$	$3.8 \times 10^9$	$7.6 \times 10^9$	$M_{\odot}$

90% of the predicted X-ray luminosity would originate within 50 kpc of the center of NGC6251 for the "halo" component, and within 1 kpc for the "core" component ↗

Divide luminosities by 1.352

$$M_{89} \sim 1.5 \times 10^{43}$$

## Table 5

Parameters of field models fitted to transverse intensity and polarization profiles (see figure 30)

	$(H) = 32''$	$(H) = 227''$
Field Pitch angle $\psi_R$	$48^\circ$	$14^\circ$
Inclination of jet to sky	$5^\circ$	$40^\circ$
Random field magnitude	$0.75 B_0$	$0.35 B_0$
Relativistic particle distribution (density)	Uniform	Gaussian $\sigma = 0.94R$
Relativistic particle distribution (pitch angle)	Isotropic	Isotropic

Mass in the berric RM median.

$\Delta RM \sim 70 \text{ rad/m}^2$  across  $L \sim 70'' \sim 30 \text{ kpc}$ .

$$\text{So: } RM = 8.1 \times 10^5 \times \bar{n}_e \times 10^{-6} B_{-6} \times 30 \times 1000$$

$$\bar{n}_e = 0.00288 \text{ cm}^{-3}$$

$$\bar{\rho}_e = \bar{n}_e m_p \sim 4.818 \times 10^{-24} \text{ kg/m}^3$$

$$M = \frac{4}{3} \pi \bar{\rho}_e R^3$$

$$= \frac{4}{3} \times \pi \times 4.818 \times 10^{-24} \times (3 \times 10^4 \times 3.0857 \times 10^{16})^3$$

$$= \frac{1.60 \times 10^{40}}{B_{-6}} \text{ kg}$$

$$= \frac{8.0 \times 10^9 M_{\odot}}{B_{-6}}$$

27 September 1982

Check Rick's ARM limit to  $n_e$ .

Take  $\theta \sim 240''$      $\Delta RM < 5 \text{ rad/m}^2$   
 $B_{eq} \sim 9 \times 10^{-6} \text{ gauss}$   
 $\Phi \sim .14'' \sim 6000 \text{ pc}$

$$RM = 8.1 \times 10^5 n_e (\text{cm}^{-3}) B (\text{gauss}) L_{pc} \text{ rad/m}^2$$

$$n_e < \frac{5}{8.1 \times 10^5 \times 9 \times 10^{-6} \times 6000} < 1.1 \times 10^{-4} \text{ cm}^{-3} \quad \checkmark$$

If  $B_{\parallel} \sim B_{\perp} \sim B_{eq}$ !

Try actual CH config?     $\theta = 227''$

From the CH fit, FWHM of convolved jet =  $42.4 + 27.7 = 70.1$  units  
 normalisation of compute units is  $\frac{1}{70.1} \times 13.4 \times 0.429 \text{ kpc}$   
 $= 0.082 \text{ kpc/cell} = 82 \text{ pc/cell}$

$$\text{Now put } B_{eq} \sim \sqrt{B_{CH}^2 + B_{rand}^2} \sim \sqrt{\left(\frac{1}{2} B_0\right)^2 + (0.35 B_0)^2}$$

$$= 0.61 B_0 = 9 \times 10^{-6} \text{ gauss}$$

$$B_0 = 14.7 \times 10^{-6} \text{ gauss}$$

Hence  $ROT = 8.1 \times 10^5 n_e (\text{cm}^{-3}) \times 0.04 \times 14.7 \times 10^{-6} \times 82$   
 $= 39.05 n_e$

$$ROT = 0.0075 \equiv 1.9 \times 10^{-4} \text{ cm}^{-3}$$

Out at  $\theta \sim 227$

$n_{eT} \sim 2 \times 10^3$  [from the pressure curve fit to complement]

$T \sim 3 \times 10^{-7} \sim n_e \sim \frac{2}{3} \times 10^{-4}$

$\sim 6 \times 10^{-5} \text{ cm}^{-3}$  [we used this for  $\theta = 240^\circ$ ]

Rick's farad. est is  $< 1.4 \times 10^{-4} \text{ cm}^{-3}$  [OK] ✓

From the equipartition sun,  $n_{eT} \sim 1 \times 10^4$  <sup>between</sup> in the knots;  $\sim 2$  higher <sup>within them?</sup>

$\rightarrow n_e \sim 3 \times 10^{-4} \text{ cm}^{-3}$

Correct to minimum from the "min. pers. cylinder" calculation [Over/Burns]?



19 Aug 1982

Analysis of JETIX output on "NGC6251"  $\odot = 32^\circ$ .

The parameter we specify is ROT

$$\text{FARAD} = \text{ROT} * \text{NCD} * \text{BPARL} * \text{W} / \text{COS I} \quad (\text{radians}).$$

i.e. it is the Faraday depth of a cell 1 unit thick

$$n_e = n_e(\text{max})$$

$$B = B_R (\text{max at edge of jet})$$

All Faraday depths then scale to this.

$$\text{ROT} = 8.1 \times 10^5 n_e(\text{cm}^{-3}) \lambda_{\text{metres}}^2 B(\text{gauss}) [\text{Lengths along l.o.s. in pc}]$$

$$\text{Cellwidth } W = 4R / (2NL - 1) \quad \text{Now } NL = 1301$$

$$R = 60$$

$$W = 0.0922 \quad 1301 \text{ of them} \rightarrow \text{Total depth of } \underline{\underline{120}} \checkmark$$

Now from the CH fit, FWHM of convolved jet =  $47 + 49 = \underline{\underline{96 \text{ units}}}$

i.e. the normalisation here is that computer units are  $\frac{1}{96} \times 3.75 \times 0.429 \text{ kpc}$

$$= 0.01676 \text{ kpc}$$

$$= \underline{\underline{16.76 \text{ pc}}}$$

$$\begin{aligned} \text{Now put } B_{\text{eq}} &\sim \sqrt{B_{\text{CH}}^2 + B_{\text{rand}}^2} = \sqrt{\left(\frac{1}{2} B_0\right)^2 + (0.75 B_0)^2} \\ &= 0.90 B_0 \end{aligned}$$

$$B_{\text{eq}} = 2.4 \times 10^{-5} \text{ gauss}$$

$$B_0 = 2.67 \times 10^{-5} \text{ gauss.}$$



Then here  $ROT = 8.1 \times 10^5 n_e (\text{cm}^{-3}) \times 0.04 \times 2.67 \times 10^{-5} \times 16.76$   
 $= 14.5 n_e$ .

Hence  $ROT = 0.02$   $n_e = 1.38 \times 10^{-3} \text{ cm}^{-3}$   $37\% \rightarrow 10\%$  over profile  
 $\Delta PA \quad 23^\circ \rightarrow -17^\circ = 40\%$

$= 0.04$   $2.75 \times 10^{-3} \text{ cm}^{-3}$   $37\% \rightarrow 1\%$   
 $\Delta PA \quad 28^\circ - 34^\circ \quad 61^\circ$

[beginning of the first bounce]

$= 0.06$   $4.13 \times 10^{-3} \text{ cm}^{-3}$   $32\% \rightarrow 7\%$   
 $\Delta PA \quad 57^\circ - 66^\circ \quad \underline{123^\circ !}$

[well-developed bounce]

$= 0.10$   $6.89 \times 10^{-3} \text{ cm}^{-3}$   $All < 20\%$   
 This is not seen  $\Delta PA \quad +70^\circ, -90^\circ \text{ noisy } \underline{\underline{160^\circ!!}}$

If we had used Croffri + Jones (1980) we would have  
concluded that for  $D > 0.8$  we would need  $F_c \leq 2.6$

i.e., in their units  $2fR < 2.6$

$$f = 1600 n_e B \lambda^2 \text{ m}^2/\text{m}^2/\text{kpc}$$

i.e.  $1600 n_e B \lambda^2 \cdot (1.61) < 2.6$

$$n_e < \frac{2.6}{1.61} \times \frac{1}{24 \times 0.04} \times \frac{1}{1600}$$

$$< \underline{\underline{1.1 \times 10^{-3} \text{ cm}^{-3}}}$$

Suppose we had done it from the slab model as for NGC 315 in Willis et al. (1981).

$$D \sim \frac{\lambda_2^2 \sin(RM \lambda_1^2)}{\lambda_1^2 \sin(RM \lambda_2^2)}$$

$$RM = 8.1 \times 10^5 \text{ } n_e (\text{cm}^{-3}) \text{ } B (\text{gauss}) \text{ } L^{-pc} \text{ } \text{rad/m}^2$$

We want  $D > 0.8$  (say).

$$\begin{aligned} \lambda_2 &= 6 \text{ cm} \\ \lambda_1 &= 20 \text{ cm} \end{aligned}$$

$$D = 9 \times 10^{-2} \frac{\sin(RM \lambda_1^2)}{\sin(RM \lambda_2^2)}$$

$$\text{If } RM = 8.1 \times 10^5 n_e \times \frac{2.4 \times 10^{-5}}{\sqrt{3}} \times 1610 = \frac{1.81}{3.13} \times 10^4 n_e (\text{cm}^{-3})$$

$$\text{Then } n_e = 10^{-4} \rightarrow RM = 1.81$$

$$D = 1.00$$

$$n_e = 10^{-3} \rightarrow RM = 18.1$$

$$D = 0.92$$

So we would have concluded that  $D > 0.8$  needs  $n_e > \frac{1.6 \times 10^{-3}}{RM} ?$

$$RM = 28.4$$

This would be  $\sim 1.6$  less than we got from the randomized CH sum.

If we used  $n_e = 4 \times 10^{-3} \text{ cm}^{-3}$  here, we would get  $RM = 125.2$

$$D = 0.2 !!$$

Conclude from these simulations that  $n_e(32'') \lesssim 4 \times 10^{-3} \text{ cm}^{-3}$

We used  $n(240'') = 6 \times 10^{-5}$

$\rightarrow n(32'') = 26.5 \times 6 \times 10^{-5}$  from BCH ratios  
 $= 1.6 \times 10^{-3} \checkmark$

$\therefore$  we are OK for Hardee.

cf. Slab approach  $n < ~~1.6~~ \times 10^{-3}$

Cioffi/Jones  $n < 1.1 \times 10^{-3}$



NGC 6251 " 1.30 resolution "

1662 MHz

D = 92.4 mpc  
 $\alpha = 0.7$   
 10 MHz  $\rightarrow$  10 GHz

VAX-fitted slice parms

$\times 0.86 \rightarrow \frac{m}{p}$

$\downarrow$   
 $m^{-3} \rightarrow m^{-3} \times 10^3$

Slice	$\theta$ (")	$m_{\text{Jy}}$ $I_{\text{max}}$	$\Phi$ (")	$\Phi_0$	$\Delta$ (")	$B_{\text{eq}}$	$U_{\text{min}}$	$n_{\text{eq}}$
1	0	41.9	1.413 ± 0.04		-0.0004			
2	1.1	61.7	1.429 ± 0.05		-0.0028			
3	2.2	3.089	1.510 ± 0.33		-0.036			
4	3.3	2.83	1.384 ± 0.32		-0.073			
5	4.4	3.21	1.43 ± 0.29		-0.173			
6	5.5	4.50	1.47 ± 0.17	(0.69)	-0.128			
7	6.6	3.49	1.58 ± 0.22	0.90	-0.111			
8	7.7	1.67	1.63 ± 0.52	0.98	-0.266			
9	8.8	1.02	1.68 ± 0.77	1.06	-0.408	27.3 ← 24.3	$5.5 \times 10^{-12}$	$1.4 \times 10^1$
10	9.9	1.55	2.04 ± 0.59	1.57	-0.414	24.5	$5.6 \times 10^{-12}$	$1.4 \times 10^1$
11	11.0	2.34	1.88 ± 0.41	1.36	-0.383	28.7	$7.7 \times 10^{-12}$	$1.9 \times 10^1$
12	12.1	2.93	1.99 ± 0.36	1.51	-0.415			
13	13.2	3.32	2.39 ± 0.35	2.01	-0.256	28.4	$7.5 \times 10^{-12}$	$1.9 \times 10^1$
14	14.3	3.13	2.31 ± 0.30	1.91	-0.359			
15	15.4	2.51	2.42 ± 0.37	2.04	-0.265			
16	16.5	1.84	3.14 ± 0.66	2.86	-0.217	21.7	$4.4 \times 10^{-12}$	$1.1 \times 10^1$
17	17.6	2.69	3.30	3.03	-0.087			
18	18.7	3.19	3.58	3.34	-0.335			
19	19.8	3.39	3.37	3.11	-0.292			
20	20.9	3.13	3.16	2.88	-0.489			
21	22.0	3.42	3.10	2.81	-0.402			
22	23.1	3.83	3.32	3.05	-0.295			
23	24.2	3.94	3.20	2.92	-0.168			
24	25.3	3.98	3.08	2.79	-0.189			
25	26.4	4.03	3.05	2.76	-0.290	27.4	$7.0 \times 10^{-12}$	$1.8 \times 10^1$
26	27.5	3.31	3.16	2.88	-0.328			
27	28.6	2.55	3.39	3.13	-0.484			
28	29.7	2.30	4.27	4.07	-0.234			
29	30.8	2.72	3.82	3.59	-0.259			
30	31.9	3.18	3.69	3.45	-0.250	24.0	$5.4 \times 10^{-12}$	$1.4 \times 10^1$
31	33.0	2.70	3.66	3.42	-0.304			
32	34.1	1.93	4.30	4.10	-0.263			
33	35.2	2.10	4.09	3.88	-0.190			
34	36.3	1.97	4.41	4.21	-0.504			
35	37.4	1.67	4.09	3.88	-0.533			
36	38.5	1.10	5.02	4.85	-0.998	16.1	$2.4 \times 10^{-12}$	$6.1 \times 10^0$
37	39.6	0.978	4.23	4.03	-0.977			
38	40.7	1.16	4.63	4.44	-0.839			
39	41.8	1.15	5.35	5.19	-0.701			
40	42.9	1.11	4.75	4.57	-0.625			
41	44.0	1.02	4.53	4.34	-0.922			
42	45.1	1.38	5.03	4.86	-0.478			
43	46.2	1.64	4.79	4.61	-0.408			
44	47.3	1.65	5.05	4.85	-0.361			
45	48.4	2.56	4.56	4.37	-0.276			
46	49.5	3.05	4.41	4.21	-0.229	22.4	$4.7 \times 10^{-12}$	$1.2 \times 10^1$
47	50.6	2.34	4.84	4.66	-0.148			
48	51.7	1.75	5.39	5.23	-0.229			
49	52.8	1.29	5.46	5.30	-0.372			
50	53.9	1.18	4.95	4.78	-0.697			



1"3

	$\theta(^{\circ})$	$I_{max}$	$\bar{I}^{\prime\prime}$	$\bar{I}_0$		$\Delta(^{\circ})$		$B_{eff}$	$u_{min}$	$nT$
51	55.0	1.04	4.61	4.42		-0.821				
52	56.1	1.07	4.03	3.81		-0.823				
53	57.2	0.889	4.11	3.90		-0.724	16.1		$2.4 \times 10^{-12}$	$6.1 \times 10^1$
54	58.3	0.387	2.01			+0.841				
55	59.4	0.709	6.95	6.83		-0.541				
56	60.5	1.01	5.47	5.31		-0.614				
57	61.6	0.936	5.10	4.93		-0.815				
58	62.7	1.01	4.88	4.70		-0.978				
59	63.8	1.14	4.50	4.31		-1.043	16.8		$2.6 \times 10^{-12}$	$6.7 \times 10^1$
60	64.9	1.13	5.19	5.02		-0.914				
61	66.0	0.904	7.02	6.90		-1.067				
62	67.1	0.860	4.95	4.78		-1.700				
63	68.2	1.086	5.44	5.28		-1.247				
64	69.3	1.29	5.30	5.14		-1.459				
65	70.4	1.56	4.85	4.67		-1.436				
66	71.5	1.67	4.41	4.21		-1.247	18.9		$3.3 \times 10^{-12}$	$8.4 \times 10^1$
67	72.6	1.61	4.17	3.96		-1.385				
68	73.7	1.61	4.43	4.23		-1.429				
69	74.8	1.51	4.26	4.06		-0.875				
70	75.9	1.52	4.02	3.80		-1.148				
71	77.0	1.55	4.22	4.01		-1.380				
72	78.1	1.20	6.65	6.52		-1.173				
73	79.2	1.14	5.64	5.49		-1.316				
74	80.3	1.09	5.38	5.22		-0.753	15.7		$2.3 \times 10^{-12}$	$5.8 \times 10^1$
75	81.4	0.981	5.70	5.55		-0.876				
76	82.5	1.28	5.55	5.40		-0.869				
77	83.6	1.71	4.70	4.52		-0.990				
78	84.7	2.04	4.78	4.60		-0.784	19.5		$3.5 \times 10^{-12}$	$9.0 \times 10^1$
79	85.8	1.85	4.93	4.76		-0.398				
80	86.9	1.86	4.56	4.37		-0.370				
81	88.0	1.65	5.00	4.83		-0.352				
82	89.1	1.32	5.19	5.02		-0.474				
83	90.2	1.15	5.36	5.20		-1.110				
84	91.3	1.18	5.68	5.53		-1.644				
85	92.4	1.02	6.07	5.93		-1.513				
86	93.5	0.945	6.01	5.87		-1.574				
87	94.6	0.860	7.19	7.07		-0.662	13.5		$1.7 \times 10^{-12}$	$4.3 \times 10^1$
88	95.7	0.908	7.22	7.10		-1.041				
89	96.8	1.086	6.13	5.99		-0.605				
90	97.9	1.050	6.21	6.07		-0.056				
91	99.0	1.241	5.99	5.85		-0.097				
92	100.1	1.49	5.67	5.52		-0.122	16.9		$2.7 \times 10^{-12}$	$6.8 \times 10^1$
93	101.2	1.37	5.23	5.07		-0.321				
94	102.3	1.04	6.16	6.02		-0.777				
95	103.4	0.905	6.72	6.59		-0.656				
96	104.5	0.913	6.78	6.65		-0.299				
97	105.6	0.790	7.33	7.21		-0.411				
98	106.7	0.888	6.57	6.44		-0.396				
99	107.8	0.980	6.11	5.97		-0.201				



NEC6251 1662 MHz 2" 11 respec..

SLICE	$\theta''$	$I_{max}$	$\Phi''$	$\Phi_0$	equiv $I_{1.3}$	$\Delta''$			
1	0	4.32							
2	1.5	111.5				-0.0022			
3	3	6.74				-0.0422			
4	4.5	5.87	2.24	0.75	2.23	-0.138			
5	6	6.78	2.31	0.94	2.57	-0.132			
6	7.5	3.75	2.38	1.10	1.42	-0.208			
7	9	2.29	2.47	1.28	0.87	-0.358			
8	10.5	3.66	2.61	1.36	1.39	-0.401			
9	12	5.54	2.75	1.76	2.10	-0.370			
10	13.5	6.33	3.07	2.23	2.40	-0.290			
11	15	5.68	2.99	2.12	2.16	-0.296			
12	16.5	4.72	3.46	2.74	1.79	-0.115			
13	18	6.64	3.89	3.27	2.52	-0.239			
14	19.5	7.72	3.83	3.20	2.93	-0.320			
15	21	7.38	3.60	2.92	2.80	-0.398			
16	22.5	8.17	3.64	2.97	3.10	-0.324			
17	24	8.84	3.68	3.02	3.36	-0.227			
18	25.5	9.03	3.62	2.94	3.43	-0.200			
19	27	8.21	3.56	2.87	3.12	-0.311			
20	28.5	6.12	3.89	3.27	2.32	-0.438			
21	30	6.03	4.17	3.60	2.29	-0.342			
22	31.5	7.09	3.94	3.33	2.69	-0.247			
23	33	6.11	4.15	3.57	2.32	-0.250			
24	34.5	4.92	4.49	3.96	1.87	-0.303			
25	36	4.70	4.47	3.94	1.78	-0.428			
26	37.5	3.69	4.68	4.18	1.40	-0.560			
27	39	2.48	5.44	5.01	0.94	-0.874			
28	40.5	2.60	5.21	4.76	0.99	-0.848			
29	42	2.82	5.30	4.86	1.07	-0.631			
30	43.5	2.66	5.08	4.62	1.01	-0.665			
31	45	3.21	5.41	4.98	1.22	-0.648			
32	46.5	4.10	5.19	4.74	1.56	-0.469			
33	48	5.36	4.97	4.50	2.03	-0.306			
34	49.5	6.52	4.86	4.38	2.48	-0.093			
35	51.0	5.27	5.14	4.69	2.00	-0.194			
36	52.5	3.55	5.68	5.27	1.35	-0.291			
37	54	2.71	5.57	5.15	1.03	-0.624			
38	55.5	2.56	4.52	(4.00)		-0.958			
39	57	2.17	4.64	(4.13)		-0.841			
40	58.5	1.78	6.24	5.87	0.68	-0.611			
41	60	2.22	5.80	5.40	0.84	-0.485			
42	61.5	2.30	5.45	5.02	0.87	-0.782			
43	63	2.53	4.86	4.38	0.96	-0.985			
44	64.5	2.76	5.12	4.67	1.05	-1.045			
45	66	2.27	6.54	(6.19)	0.86	-1.124			
46	67.5	2.27	5.76	5.36	0.86	-1.426			
47	69.0	3.26	5.26	4.82	1.24	-1.503			
48	70.5	3.81	5.13	(5.68)	1.45	-1.383			
49	72	3.91	5.04	4.58	1.48	-1.339			
50	73.5	3.78	4.98	4.51	1.44	-1.373			

#	$\theta''$	$I_{max}$	$\Phi^1$	$\Phi_0$	$I_{1.3}^{equiv}$	$\Delta''$		$S_{eq}$	$M_{min}$	$nT$
51	75	3.73	4.48	3.95	1.42	-1.082				
52	76.5	3.68	4.60	4.09	1.40	-1.216				
53	78	3.17	6.32	5.95	1.20	-1.228				
54	79.5	2.88	6.07	5.69	1.09	-1.104				
55	81	2.59	5.67	5.26	0.98	-0.942				
56	82.5	3.24	5.62	5.21	1.23	-1.034				
57	84	4.31	5.20	4.75	1.64	-0.840				
58	85.5	4.66	5.15	4.70	1.77	-0.517				
59	87	4.26	5.20	4.75	1.62	-0.381				
60	88.5	3.59	5.56	5.14	1.36	-0.409				
61	90	2.84	6.01	5.63	1.08	-0.818				
62	91.5	2.75	6.39	6.03	1.04	-1.383	14.9	$2.1 \times 10^{-12}$	$5.2 \times 10^1$	
63	93	2.58	6.39	6.03	0.98	-1.334				
64	94.5	2.21	7.16	6.81	0.84	-0.941				
65	96	2.46	7.31	7.50	0.93	-0.882				
66	97.5	2.75	6.89	6.56	1.04	-0.482				
67	99	3.24	6.26	5.89	1.23	-0.173				
68	100.5	3.52	5.95	5.56	1.34	-0.277				
69	102	2.77	6.22	5.85	1.05	-0.614				
70	103.5	2.44	7.05	6.72	0.93	-0.511				
71	105	2.33	7.29	6.98	0.88	-0.379	13.6	$1.7 \times 10^{-12}$	$4.4 \times 10^1$	
72	106.5	2.33	7.08	6.76	0.88	-0.447				
73	108	2.68	6.40	6.04	1.02	-0.432				
74	109.5	3.16	6.23	5.86	1.20	-0.538				
75	111	2.81	7.06	6.74	1.07	-0.687				
76	112.5	2.38	7.72	7.43	0.90	-0.521	13.5	$1.7 \times 10^{-12}$	$4.3 \times 10^1$	
77	114	2.58	7.66	7.36	0.98	+0.211				
78	115.5	2.11	8.64	8.38	0.80	+0.301	12.6			
79	117	1.73	9.56	9.32	0.66	0.464	11.5	$1.2 \times 10^{-12}$	$3.1 \times 10^1$	
80	118.5	1.61	8.71	8.45	0.61	0.397				
81	120.0	1.53	8.86	8.61	0.58	0.508				
82	121.5	1.33	9.64	9.41	0.50	0.420	10.6	$1.1 \times 10^{-12}$	$2.7 \times 10^1$	
83	123	1.13	13.29	(13.12)	0.43	0.307				
84	124.5	1.17	15.07	(14.92)		0.474				
85	126	1.13	11.81	11.62	0.43	0.144	10.0	$9.4 \times 10^{-13}$	$2.4 \times 10^1$	
86	127.5	0.962	12.67	12.49	0.37	0.167	8.95	$7.5 \times 10^{-13}$	$1.9 \times 10^1$	
87	129	0.85	14.38	14.22	0.32	-0.346	8.33	$6.5 \times 10^{-13}$	$1.6 \times 10^1$	
88	130.5	0.987	14.24	14.08	0.37	0.177				
89	132	0.985	13.17	13.0	0.37	0.678	8.91	$7.4 \times 10^{-13}$		
90	133.5	0.901	12.83	12.66	0.34	0.702				



NGC 6251 "4.39 resolution"

1662 MHz  
Cell size = ~~1.5~~ 3".S

SUCE	$\theta$ (")	$I_{max}$	$\Phi$ (")	<del>4.39</del> $\Phi_0$	$\Delta$ (")	$I_{1.3}^{equiv}$	Beam negative	$U_{min}$ $J_{m-3}$	$n_T$ $m^{-3}K$
1	0	43.19	4.75	<del>0.50</del>	1.81	-0.00078			
2	3.5	85.1	4.78	<del>0.53</del>	1.89	-0.0199			
3	7.0	10.0	4.84	<del>0.53</del>	2.04	-0.189			
4	10.5	9.07	5.08	<del>1.80</del>	2.56	-0.363			
5	14	14.1	5.36	<del>2.48</del>	3.08	-0.320			
6	17.5	17.4	5.57	<del>2.90</del>	3.43	-0.241			
7	21	22.1	5.51	<del>2.79</del>	3.33	-0.320			
8	24.5	24.3	5.53	<del>2.83</del>	3.36	-0.270			
9	28	20.5	5.62	<del>2.99</del>	3.51	-0.316			
10	31.5	18.9	5.83	<del>3.37</del>	3.84	-0.243			
11	35	15.2	6.09	<del>3.81</del>	4.22	-0.346			
12	38.5	10.1	6.34	<del>4.20</del>	4.57	-0.604			
13	42	8.66	6.54	<del>4.56</del>	4.85	-0.697			
14	45.5	12.02	6.60	<del>4.58</del>	4.93	-0.532			
15	49	18.1	6.45	<del>4.30</del>	4.73	-0.252	1.59		
16	52.5	13.1	6.75	<del>4.80</del>	5.13	-0.314	1.15		
17	56	7.53	6.42	<del>4.32</del>	4.68	-0.705	0.660		
18	59.5	6.63	6.90	<del>5.00</del>	5.32	-0.568	0.581		
19	63	7.72	6.41	<del>4.30</del>	4.67	-0.921	0.677		
20	66.5	8.03	6.78	<del>4.84</del>	5.17	-1.205	0.704		
21	70	11.10	6.46	<del>4.38</del>	4.74	-1.369	0.973		
22	73.5	11.8	6.26	<del>4.08</del>	4.46	-1.211	1.04		
23	77	10.9	6.59	<del>4.57</del>	4.91	-1.133	0.956		
24	80.5	10.0	7.07	<del>5.24</del>	5.54	-0.953	0.877		
25	84	13.2	6.59	<del>4.57</del>	4.91	-0.732	1.16		
26	87.5	13.1	6.80	<del>4.87</del>	5.19	-0.481	1.15		
27	91	9.58	7.45	<del>5.74</del>	6.02	-0.977	0.840		
28	94.5	8.51	7.71	<del>6.07</del>	6.34	-0.988	0.746		
29	98	10.2	7.48	<del>5.78</del>	6.06	-0.434	0.894		
30	101.5	10.3	7.31	<del>5.86</del>	5.84	-0.390	0.903		
31	105	8.50	7.90	<del>6.31</del>	6.57	-0.477	0.745		
32	108.5	9.61	7.47	<del>5.77</del>	6.04	-0.464	0.843		
33	112	9.42	8.04	<del>6.49</del>	6.74	-0.405	0.826		
34	115.5	7.75	8.65	<del>7.23</del>	7.45	+0.224	0.680		
35	119	5.79	9.27	<del>7.90</del>	8.16	0.344	0.508		
36	122.5	4.82	10.03	<del>8.83</del>	9.02	0.118	0.423		
37	126	4.05	10.36	<del>9.21</del>	9.38	0.110	0.355		
38	129.5	3.39	10.54	<del>9.41</del>	9.58	0.343	0.297		
39	133	3.38	10.65	<del>9.53</del>	9.7	0.946	0.296		
40	136.5	3.71	11.77	<del>10.77</del>	10.92	0.927	0.325		
41	140	5.05	9.83	<del>8.61</del>	8.8	-0.0006	0.443		
42	143.5	5.07	9.12	<del>7.79</del>	7.99	-0.159	0.445	9.07	$7.68 \times 10^{-13}$
43	147	3.96	10.29	<del>9.13</del>	9.31	-0.103	0.347		$1.94 \times 10^{-11}$
44	150.5	3.14	10.85	<del>9.75</del>	9.92	+0.191	0.275		
45	154	2.62	10.64	<del>8.52</del>	9.69	+0.393	0.230		
46	157.5	2.68	11.38	<del>10.54</del>	10.50	+0.338	0.235		
47	161	2.67	12.25	<del>11.29</del>	11.44	+0.339	0.234		
48	164.5	2.18	14.32	<del>13.81</del>	13.63	+0.150	0.191	6.52	$2.58 \times 10^{-13}$
49	168	2.261	13.76	<del>12.91</del>	12.14	-0.459	0.198		$6.52 \times 10^9$
50	171.5	2.1	11.92	<del>10.94</del>	11.09	+0.231	0.229		

↑  
haw

↑  
central

NGC 6251

4.39 masel

1662 MHz  
Cell ~~15~~ 3.5

SLICE	$\theta$	$I_{max}$	$\Phi$ (")	$\Phi_0$	$\Delta$ (")	$I_{1.3}^{equiv}$	$B_{eq}$	$4\pi m_i$	$\tau T$
51	175	3.68	12.54	11.75	+0.679	0.323			
52	178.5	5.18	11.27	10.38	+0.693	0.454			
53	182	6.52	10.64	9.69	-0.296	0.572			
54	185.5	6.91	9.89	8.86	-0.585	0.606			
55	189	7.82	9.66	8.60	-1.162	0.686			
56	192.5	9.90	9.26	8.15	-1.114	0.868	10.9	$1.10 \times 10^{-12}$	$2.78 \times 10^{10}$
57	196	8.10	10.48	9.51	-0.983	0.710			
58	199.5	6.25	11.30	10.4	-0.414	0.548	8.28	$6.41 \times 10^{-13}$	$1.62 \times 10^{10}$
59	203	7.70	12.37	11.56	+0.941	0.675			
60	206.5	16.0	10.29	9.31	+1.114	1.403			
61	210	17.5	10.12	9.12	0.959	1.54	12.0	$1.34 \times 10^{-12}$	$3.39 \times 10^{10}$
62	213.5	11.4	11.29	10.40	-0.304	1.00			
63	217	6.82	13.0	12.23	-1.583	0.598	7.74	$5.60 \times 10^{-13}$	$1.42 \times 10^{10}$
64	220.5	7.64	13.6	12.87	-1.529	0.670			
65	224	11.20	13.3	12.6	-1.801	0.982			
66	227.5	13.9	13.4	12.7	-1.632	1.219			
67	231	14.1	12.7	11.9	-1.791	1.24	9.67	$8.74 \times 10^{-13}$	$2.21 \times 10^{10}$
68	234.5	10.4	13.3	12.6	-1.561	0.912			
69	238	8.17	16.4	15.8	+0.247	0.716	7.04	$4.63 \times 10^{-13}$	$1.17 \times 10^{10}$
70	241.5	10.85	15.1	14.4	+0.999	0.951			
71	245	10.65	14.7	14.0	1.404	0.934			
72	248.5	9.68	15.0	14.3	2.397	0.849			
73	252	8.83	14.7	14.0	3.787	0.774	10.7	$1.08 \times 10^{-12}$	$2.7 \times 10^{10}$
74	255.5	7.23	14.3	13.6	4.580	0.634			
75	259	5.15	16.0	15.4	5.800	0.450			
76	262.5	3.24	18.1	17.6	7.555	0.284	5.08	$2.41 \times 10^{-13}$	$6.1 \times 10^9$
77	266	2.56	17.9	17.4	9.350	0.224			
78	269.5	1.82	19.2	18.7	10.22	0.160			
79	273	1.31	21.9	21.5	11.05	0.115			
80	276.5	1.27	19.3	18.8	11.58	0.111	3.74	$1.31 \times 10^{-13}$	$3.31 \times 10^9$

# HBC turbulence - NEC6251

$\Theta$	$\Phi$	$d\Phi/d\Theta$	$\langle d\Phi/d\Theta \rangle$	$\langle \rangle^3$	$v_j$	$v_j/\Phi$	$(v_j/\Phi)^2$	$\langle \rangle^2 ( )^2$	$\log_{10}$
1.6	(0.12)								
2.0	(0.1278)	0.020	0.020	$8 \times 10^{-6}$	1.33	$1.04 \times 10^1$	$1.08 \times 10^2$	$8.66 \times 10^{-4}$	-3.06
3	(0.1826)	0.055	0.055	$1.66 \times 10^{-4}$	1.80	9.59	97.2	$1.61 \times 10^{-2}$	-1.79
4	(0.25)	0.074	0.074	$4.05 \times 10^{-4}$	2.05	7.98	63.6	$2.58 \times 10^{-2}$	-1.59
5	(0.35)	0.093	0.093	$8.04 \times 10^{-4}$	2.17	6.20	38.4	$3.09 \times 10^{-2}$	-1.51
6	(0.50)	0.15	0.15	$3.38 \times 10^{-3}$	2.26	4.52	20.4	$6.91 \times 10^{-2}$	-1.16
7	(0.85)	0.35	0.35	$4.29 \times 10^{-2}$	2.32	2.73	7.45	$3.20 \times 10^{-1}$	-0.49
9	1.35	0.25	0.20	$8 \times 10^{-3}$	2.38	1.76	3.11	$2.49 \times 10^{-2}$	-1.60
11	1.55	0.10	0.175	$5.36 \times 10^{-3}$	2.43	1.57	2.46	$1.32 \times 10^{-2}$	-1.88
15	2.25	0.15	0.15	$3.38 \times 10^{-3}$	2.475	1.15	1.33	$4.48 \times 10^{-3}$	-2.35
17	2.60	0.225	0.15	$3.38 \times 10^{-3}$	2.487	0.957	0.915	$3.09 \times 10^{-3}$	-2.51
19	2.85	0.125	0.13	$2.20 \times 10^{-3}$	2.49	0.874	0.763	$1.68 \times 10^{-3}$	-2.78
21	2.95	0.050	0.09	$5.12 \times 10^{-4}$	2.493	0.845	0.714	$3.66 \times 10^{-4}$	-3.44
23	3.00	0.025	0.03	$2.70 \times 10^{-5}$	2.4935	0.831	0.691	$1.87 \times 10^{-5}$	-4.73
25	3.00	0.050	0.0	0.00					
27	3.05	0.025	0.025	$1.56 \times 10^{-5}$	2.485	0.815	0.664	$1.04 \times 10^{-5}$	-4.99
29	3.25	0.100	0.07	$3.43 \times 10^{-4}$	2.48	0.763	0.582	$2.00 \times 10^{-4}$	-3.70
31	3.40	0.075	0.09	$7.29 \times 10^{-4}$	2.475	0.728	0.530	$3.86 \times 10^{-4}$	-3.41
33	3.65	0.125	0.125	$1.95 \times 10^{-3}$	2.472	0.677	0.459	$8.94 \times 10^{-4}$	-3.05
35	3.90	0.125	0.125	$1.95 \times 10^{-3}$	2.473	0.634	0.402	$7.84 \times 10^{-4}$	-3.11
37	4.10	0.100	0.110	$1.33 \times 10^{-3}$	2.478	0.604	0.365	$4.86 \times 10^{-4}$	-3.31
39	4.35	0.125	0.110	$1.33 \times 10^{-3}$	2.486	0.572	0.327	$4.34 \times 10^{-4}$	-3.36
41	4.50	0.075	0.08	$5.12 \times 10^{-4}$	2.49	0.553	0.306	$1.57 \times 10^{-4}$	-3.81
43	4.60	0.050	0.06	$2.16 \times 10^{-4}$	2.50	0.544	0.295	$6.38 \times 10^{-5}$	-4.20
45	4.70	0.050	0.05	$1.25 \times 10^{-4}$	2.51	0.534	0.285	$3.56 \times 10^{-5}$	-4.45
47	4.80	0.050	0.05	$1.25 \times 10^{-4}$	2.515	0.524	0.275	$3.43 \times 10^{-5}$	-4.46
49	4.85	0.025	0.025	$1.56 \times 10^{-5}$	2.52	0.520	0.270	$4.21 \times 10^{-6}$	-5.38
51	4.90	0.025	0.025	$1.56 \times 10^{-5}$	2.523	0.515	0.265	$4.14 \times 10^{-6}$	-5.38
53	4.95	0.025	0.025	$1.56 \times 10^{-5}$	2.527	0.511	0.261	$4.07 \times 10^{-6}$	-5.39
55	4.97	0.010	0.010	$1.00 \times 10^{-6}$	2.531	0.509	0.259	$2.59 \times 10^{-7}$	-6.59
57	4.99	0.010	0.010	$1.00 \times 10^{-6}$	2.531	0.507	0.257	$2.57 \times 10^{-7}$	-6.59
59	5.00	0.005	0.005	$1.25 \times 10^{-7}$	2.532	0.506	0.256	$3.21 \times 10^{-8}$	-7.49
80	5.05	0.0024	0.0024	$1.38 \times 10^{-8}$	2.53	0.501	0.251	$3.46 \times 10^{-9}$	-8.46
82	5.1	0.025	0.025	$1.56 \times 10^{-5}$	2.53	0.496	0.246	$3.84 \times 10^{-6}$	-5.42
84	5.2	0.050	0.050	$1.25 \times 10^{-4}$	2.532	0.487	0.237	$2.96 \times 10^{-5}$	-4.53
86	5.32	0.060	0.060	$2.16 \times 10^{-4}$	2.534	0.476	0.227	$4.90 \times 10^{-5}$	-4.31
88	5.53	0.105	0.105	$1.16 \times 10^{-3}$	2.535	0.458	0.210	$2.44 \times 10^{-4}$	-3.61
90	5.74	0.105	0.105	$1.16 \times 10^{-3}$	2.537	0.442	0.195	$2.27 \times 10^{-4}$	-3.64
92	6.0	0.13	0.13	$2.20 \times 10^{-3}$	2.54	0.423	0.179	$3.94 \times 10^{-4}$	-3.40
94	6.4	0.20	0.20	$8.00 \times 10^{-3}$	2.542	0.397	0.158	$1.26 \times 10^{-3}$	-2.90
96	6.6	0.20	0.10	$1.00 \times 10^{-3}$	2.545	0.386	0.149	$1.47 \times 10^{-4}$	-3.83
98	6.4	0.10	0.10	$1.00 \times 10^{-3}$	2.548	0.398	0.159	$1.59 \times 10^{-4}$	-3.80
100	6.1	0.15	0.125	$3.45 \times 10^{-3}$	2.551	0.418	0.175	$3.01 \times 10^{-4}$	-3.52
102	5.9	0.15	0.15	$3.38 \times 10^{-3}$	2.553	0.440	0.194	$6.54 \times 10^{-4}$	-3.18
104	6.25	0.225	0.225	$1.14 \times 10^{-2}$	2.555	0.409	0.167	$1.51 \times 10^{-3}$	-2.72
106	6.8	0.275	0.275	$2.08 \times 10^{-2}$	2.557	0.376	0.141	$2.94 \times 10^{-3}$	-2.53
108	6.3	0.25	0.27	$1.56 \times 10^{-2}$	2.559	0.406	0.165	$2.57 \times 10^{-3}$	-2.59
110	5.8/6.3	0.25	0.26	$1.56 \times 10^{-2}$	2.561	0.416	0.173	$2.70 \times 10^{-3}$	-2.57
112	6.8	0.25	0.25	$1.56 \times 10^{-2}$	2.563	0.376	0.142	$2.21 \times 10^{-3}$	-2.65
114	7.25	0.225	0.25	$1.14 \times 10^{-2}$	2.565	0.354	0.125	$1.43 \times 10^{-3}$	-2.85
116	7.9	0.325	0.30	$3.43 \times 10^{-2}$	2.567	0.325	0.106	$3.62 \times 10^{-3}$	-2.44

HBC turbulence - NCG 251 cont'd.

$\ominus$	$\Phi$	$ d\Phi/d\Theta $	$\langle \rangle$	$\langle \rangle^2$	$v_j$	$(v_j/\Phi)$	$(\ )^2$	$\langle \rangle^3 (\ )^2$	$10_{10}$
118	8.4	0.25	0.25	1.56 $10^{-2}$	2.568	0.306	0.093	1.46 $10^{-3}$	-2.84
120	8.7	0.15	0.16	4.10 $10^{-3}$	2.568	0.295	0.087	3.57 $10^{-4}$	-3.45
122	8.95	0.125	0.14	2.74 $10^{-3}$	2.569		0.082	2.25 $10^{-4}$	-3.65
124	9.2	0.125	0.125	1.95 $10^{-3}$	2.57	0.279	0.078	1.52 $10^{-4}$	-3.82
126	9.4	0.10	0.10	1 $10^{-3}$	2.571	0.274	0.075	7.48 $10^{-5}$	-4.13
128	9.55	0.05	0.08	5.12 $10^{-4}$	2.571		0.073	3.75 $10^{-5}$	-4.43
130	9.65	0.075	0.06	2.16 $10^{-4}$	2.572	0.267	0.071	1.53 $10^{-5}$	-4.81
132	9.70	0.025	0.03	2.70 $10^{-5}$	2.573		0.070	1.90 $10^{-6}$	-5.72
134	9.70	0.050	0.00	—	2.574				
136	9.60	0.05	0.05	1.25 $10^{-4}$	2.575	0.268	0.072	8.99 $10^{-6}$	-5.05
138	9.4	0.1	0.1	10 $10^{-3}$	2.576	0.274	0.075	7.51 $10^{-5}$	-4.12
140	8.8	0.25	0.25	1.56 $10^{-2}$	6	0.269	0.084	1.31 $10^{-3}$	-2.88
142	8.4	0.25	0.25	1.56 $10^{-2}$	7			1.47 $10^{-3}$	-2.83
144	8.3	0.05	0.1	10 $10^{-3}$	7			3.1 $10^{-4}$	-3.51
146	8.45	0.075	0.06	2.16 $10^{-4}$	8		0.093	2.01 $10^{-5}$	-4.70
148	8.75	0.15	0.15	3.38 $10^{-3}$	2.578			2.93 $10^{-4}$	-3.53
150	8.15	0.2	0.18	5.83 $10^{-3}$	8			4.63 $10^{-4}$	-3.33
152	8.5	0.175	0.18	5.83 $10^{-3}$	9			4.50 $10^{-4}$	-3.37
154	9.9	0.2	0.2	8 $10^{-3}$	2.579			5.43 $10^{-4}$	-3.27
156	10.2	0.15	0.15	3.38 $10^{-3}$	9			2.16 $10^{-4}$	-3.67
158	10.8	0.3	0.15	3.38 $10^{-3}$	80			1.93 $10^{-4}$	-3.71
160	10.95	0.075	0.15	3.38 $10^{-3}$	0			1.88 $10^{-4}$	-3.73
162	11.3	0.175	0.18	5.83 $10^{-3}$	0			3.04 $10^{-4}$	-3.52
164	11.55	0.125	0.18	5.83 $10^{-3}$	2.580			2.91 $10^{-4}$	-3.54
166	11.85	0.15	0.15	3.38 $10^{-3}$	0			1.60 $10^{-4}$	-3.80
168	12.1	0.125	0.18	2.20 $10^{-3}$	1			1.00 $10^{-4}$	-4.00
170	12.25	0.075	0.1	10 $10^{-3}$	1			4.44 $10^{-5}$	-4.35
172	12.1	0.075	0.08	5.12 $10^{-4}$	1			2.33 $10^{-5}$	-4.63
174	11.8	0.15	0.15	3.38 $10^{-3}$	1			1.62 $10^{-4}$	-3.79
176	11.2	0.3	0.3	2.70 $10^{-2}$	1			1.43 $10^{-3}$	-2.84
178	10.6	0.3	0.3	2.7 $10^{-2}$	2			6.58 $10^{-3}$	-2.18
180	10.2	0.2	0.25	1.56 $10^{-2}$	2			1.0 $10^{-3}$	-3.00
182	9.8	0.2	0.2	8 $10^{-3}$	2			5.55 $10^{-4}$	-3.26
184	9.45	0.175	0.18	5.83 $10^{-3}$	2.582			4.35 $10^{-4}$	-3.36
186	9.1	0.175	0.16	4.10 $10^{-3}$	2			3.30 $10^{-4}$	-3.48
188	8.8	0.15	0.15	3.38 $10^{-3}$	2			2.97 $10^{-4}$	-3.54
190	8.45	0.175	0.13	2.20 $10^{-3}$	3			2.06 $10^{-4}$	-3.60
192	8.3	0.075	0.08	5.12 $10^{-4}$	3			4.96 $10^{-5}$	-4.30
194	8.4	0.05	0.05	1.25 $10^{-4}$	3			1.18 $10^{-5}$	-4.93
196	8.8	0.2	0.1	10 $10^{-3}$	2.583			8.62 $10^{-5}$	-4.06
198	9.6	0.4	0.3	2.7 $10^{-2}$	3			1.95 $10^{-3}$	-2.71
200	10.4	0.4	0.4	6.4 $10^{-2}$	3			3.95 $10^{-3}$	-2.40
202	11.8	0.7	0.5	1.25 $10^{-1}$	4			5.99 $10^{-3}$	-2.22
204	11.8	0.0	0.2	6.4 $10^{-2}$	4			3.07 $10^{-3}$	-2.51
206	11.5	0.15	0.2	2.7 $10^{-2}$	4			1.36 $10^{-3}$	-2.87
208	9.6	0.45	0.2	8 $10^{-3}$	2.584			5.80 $10^{-4}$	-3.24
210	9.2	0.2	0.2	8 $10^{-3}$	4			6.31 $10^{-4}$	-3.20
212	9.4	0.1	0.15	3.38 $10^{-3}$	5			2.56 $10^{-4}$	-3.59
214	10.15	0.375	0.18	5.83 $10^{-3}$	5			3.78 $10^{-4}$	-3.42
216	10.5	0.175	0.18	5.83 $10^{-3}$	6			3.59 $10^{-4}$	-3.45
218	11.3	0.1	0.1	10 $10^{-3}$	2.586			3.24 $10^{-5}$	-4.28

Fits to NRC6251 1480MHz 15"

$\Theta$	$\Delta$	$\Theta$	$\Delta$
12"	-0.016	324	+13.95
24	-0.333	336	+15.53
36	-0.381	348	+20.10
48	-0.544	360	+18.00
60	-0.672	372	+17.62
72	-1.299	384	+16.39
84	-1.193	396	+17.32
96	-0.911	408	+24.10
108	-0.611	420	+29.22
120	-0.304	432	+37.19
132	+1.304	444	+44.61
144	+1.966	456	+52.36
156	+2.103	468	+ ???
168	+4.021	480	+67.79 ?
180	-0.055	492	+61.73 ?
192	-0.810	504	+124.6
204	-0.397		
216	-0.031		
228	-1.487		
240	-0.869		
252	+1.719		
264	+4.951		
276	+9.080		
288	+11.32		
300	+11.93		
312	+14.60		

— Burbidge GR, ODen SL  
ApJ, 178, 583 (1972)

— Lake RA and Roeder RC  
JRASC, 66, 1111 (1972)

## Power Spectra of NGC6251 oscillations.

Theoretical deflection probability for random noise:

$$\Pi(P > P_0) \Rightarrow 1 - \{1 - \exp(-P_0)\}^n$$

$$\text{Where } n(k_1 < k < k_2) = \left(\frac{k_2 - k_1}{2\pi}\right)(\theta_2 - \theta_1) \quad \begin{array}{l} \theta_1 \rightarrow \theta_2 \text{ } \underline{\text{dof range}} \\ k_1 - k_2 \text{ } \underline{\text{spect range}} \end{array}$$

$$\sim 0.5 \times 98 \sim 50 \text{ in our case.}$$

$$\begin{array}{l} \text{So } \Pi \sim 1 - \exp(-50 \exp(-P_0)) \\ \sim 0.29 \text{ for } P_0 = 5 \\ \sim 0.045 \text{ for } P_0 = 7 \\ \sim 0.002 \text{ for } P_0 = 10 \end{array} \quad \text{i.e. } \left. \begin{array}{l} \sim 15 \text{ occurrences / spec.} \\ \sim 2 \text{ occurrences / spec.} \\ \sim .1 \text{ occurrence / spec.} \end{array} \right]$$

i.e.  $P(>5)$  is  $\sim 7 \times P(>7)$  (we saw  $\sim 5 \times$ ) 99.

$$P > 10 \text{ is } \sim \frac{1}{20} P(>7) \quad \boxed{\text{SAFE}}$$

For the shorter data sets,  $n \sim 0.5 \times 40 \sim 20$

$$\begin{array}{l} \Pi \sim 1 - \exp(-20 \exp(-P_0)) \\ \sim 0.13 \text{ for } P_0 = 5 \\ \sim 0.02 \text{ for } P_0 = 7 \\ \sim 0.001 \text{ for } P_0 = 10 \end{array} \quad \text{1 occurrence in 50 spectra}$$

$P = 10 \times$  mean is fairly safe, and easy to read.

Compute significances peer by peer though, key vary.



Thru send 143" 9"  
 31"  
 17.5"  
 12"

Hence:-

Average angle data  $20'' < \theta < 100''$

Peak at	0.0234	$\cdot 4199E-6$	is $\sim 7.9 \times \text{bgnd}$	$\pi = .008$	1 in 6 spectra	$\times 85$
	0.112	$\cdot 8139 E-7$	is $\sim 8.1 \times$	.006	8	$\times 17$
	0.172	$\cdot 477 E-7$	12.2x		490 spectra	$\checkmark 11$
	0.287	$\cdot 223 E-7$	16x	$2.3 \times 10^{-6}$	2151 spectra	$\checkmark 7.0$
	0.359	$\cdot 122 E-7$	28x		Unconformable	$\checkmark 5.6$

$\Rightarrow$  SIGN peaks 11".6, 7".0, 5".6

Average angle data  $0'' < \theta < 100''$

	0.292		10x bgnd	$\pi = 9.3 \times 10^{-4}$	1 in 52 spectra	$\checkmark 6".85$
	0.3575		11x	$3.4 \times 10^{-4}$	1 in 143 sp	$\checkmark 5".6$

1".3 angle data  $0'' < \theta < 100''$

	0.190		10.4x bgnd	$\pi = 1.5 \times 10^{-3}$	1 in 14 spectra	$\checkmark 5".8$
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1".3 deflection data  $0'' < \theta < 100''$

	0.190		9.3x bgnd	$\pi = 4.5 \times 10^{-3}$	1 in 4.6 spectra	$\cdot 5".8$
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2".1 angle data  $0'' < \theta < 134''$

	0.0885		7.7x bgnd	$\pi = 2.0 \times 10^{-2}$	1 in 1.2	$\times 16".9$
	0.166		11.5x bgnd	$\pi = 4.3 \times 10^{-4}$	1 in 51 spectra	$\checkmark 9".0$
	0.260		11.1x	$\pi = 6.6 \times 10^{-4}$	1 in 34	$\checkmark 5".8$

2".1 angle data  $15'' < \theta < 134''$

	0.166		16.2x bgnd	$\pi = 3.5 \times 10^{-6}$	1 in 7170	$\checkmark 9".0$
	0.266		23x			$\checkmark 5".6$
	0.31		10x		1 in 14	$\checkmark 4".8$

4" 4 angle data  $125 < \theta < 276''$

0.148

10.3 x bgnd

$\Pi = 7.4 \times 10^{-4}$

1 in 62 spectra

23".6

0.102

10.2x

$8.2 \times 10^{-2}$

1 in 56

34".3

0.274

12".7

0.372

9".4

4" 4 angle data  $180'' < \theta < 276''$

No significant peaks

15" angle data  $210'' < \theta < 440''$

← side lobes at 230'' beam aliasing

0.029

0.086

0.141

413''

140''

85''

2" 1' angle data  $30'' < \theta < 100''$

0.115

0.163

10.2 x bgnd

9.1 x bgnd

0.001

0.004

1 in 26 spectra

1 in 9 spectra

13".0

9".2

1" 3 angle data  $30'' < \theta < 100''$

0.190

0.083

0.140

26.3 x bgnd

5.8 x bgnd

5.2x

Small

$\infty$

5".8

13".3

15" angle data  $0'' < \theta < 456''$

0.0781

7.5 x bgnd

$\Pi = 0.010$

1 in 5.1 spectra

153'.6

22 July 1982

CH fit to NGC6251

$z_s = 0.6864$  (kpc)

Core integration

$a = 1.0$

$1.6 \times 10^5$  cells

$m = 4.15$

$p_s = 4 \times 10^8 \text{ cm}^{-3} \text{ K}$

$n_e T \sim 4 \times 10^8$

$R_{max} =$		$n_e = 10 \quad T = 4 \times 10^7$	$n = 20 \quad T = 2 \times 10^7$	$n = 40 \quad T = 10^7$	
1	M	$8.83 \times 10^9$	$1.77 \times 10^9$	$3.53 \times 10^9$	M
	$L_x$	$6.39 \times 10^{43}$	$2.13 \times 10^{44}$	$5.10 \times 10^{44}$	$\frac{\text{erg}}{\text{sec}}$
2		$1.44 \times 10^9$	$2.88 \times 10^9$	$5.77 \times 10^9$	
		$6.98 \times 10^{43}$	$2.33 \times 10^{44}$	$5.57 \times 10^{44}$	
10		$1.85 \times 10^9$	$3.7 \times 10^9$	$7.48 \times 10^9$	
		$6.99 \times 10^{43}$	$2.33 \times 10^{44}$	$5.58 \times 10^{44}$	
20		$1.89 \times 10^9$	$3.78 \times 10^9$	$7.58 \times 10^9$	
		$6.99 \times 10^{43}$	$2.33 \times 10^{44}$	$5.58 \times 10^{44}$	

Conclude: At  $T = 2 \times 10^7 \text{ K}$   
 Core has  $L_x \sim 2.3 \times 10^{44} \text{ erg/sec}$   
 90% within 1 kpc of center

22 July 1982

CM fit to NAC6251

$$z_s = 16.73 \text{ kpc}$$

$$a = 1.0$$

$$m = 2.60$$

Halo integration

$1.6 \times 10^5$  cells.

$$\rho_s = 4 \times 10^5 \text{ cm}^{-3} \text{ K} \quad (\text{halo})$$

$$n_e = 10^{-2} \quad T = 4 \times 10^7 \quad n_e = 2 \times 10^{-2} \quad T = 2 \times 10^7 \quad n_e = 4 \times 10^{-2} \quad T = 10^7$$

R <sub>max</sub> = 150	M	$8.41 \times 10^{10}$	$1.68 \times 10^{11}$	$3.36 \times 10^{11}$
	L <sub>x</sub>	$1.97 \times 10^{42}$	$6.56 \times 10^{42}$	$1.57 \times 10^{43}$
250	M	$1.38 \times 10^{11}$	$2.76 \times 10^{11}$	$5.52 \times 10^{11}$
	L <sub>x</sub>	$2.01 \times 10^{42}$	$6.68 \times 10^{42}$	$1.60 \times 10^{43}$
350	M	$1.77 \times 10^{11}$	$3.55 \times 10^{11}$	$7.09 \times 10^{11}$
	L <sub>x</sub>	$2.01 \times 10^{42}$	$6.70 \times 10^{42}$	$1.60 \times 10^{43}$
50	M	$4.39 \times 10^{10}$	$8.78 \times 10^{10}$	$1.76 \times 10^{11}$
	L <sub>x</sub>	$1.81 \times 10^{42}$	$6.02 \times 10^{42}$	$1.44 \times 10^{43}$

Conclude: At  $T = 2 \times 10^7$  K

Halo has  $L_x \sim 6.7 \times 10^{42}$  erg/sec

90% within 50 kpc of center

N.B. Divide L's by 1.352  
M's by 1.163

NGC6251

log-log  $\lambda_{min}(\odot)$   
( $\equiv nT$ )

$nT \text{ cm}^{-3} \text{ K}$

Minimum  $b \rightarrow$  Mult  $nT$  scale by  $0.86^{log_{10} b}$

46 7400

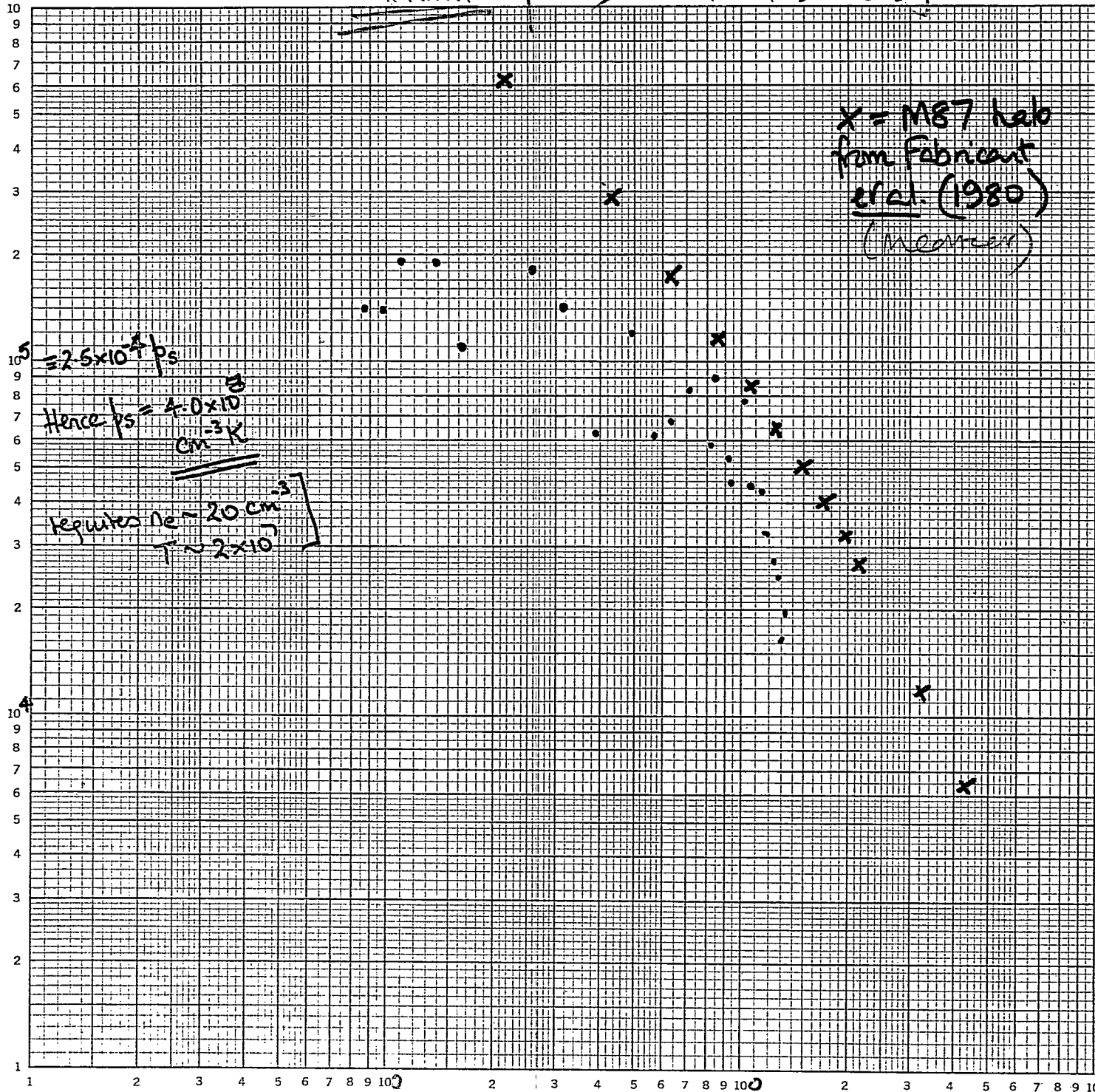
x = M87 halo  
from Fabricant  
et al. (1980)  
(mean)

$\approx 2.5 \times 10^4 \text{ ps}$

Hence  $\rho_s = 4.0 \times 10^3 \text{ cm}^{-3} \text{ K}$

requires  $n_e \sim 20 \text{ cm}^{-3}$   
 $T \sim 2 \times 10^7$

KE LOGARITHMIC 3 X 3 CYCLES  
KEUFFEL & ESSER CO. MADE IN U.S.A.

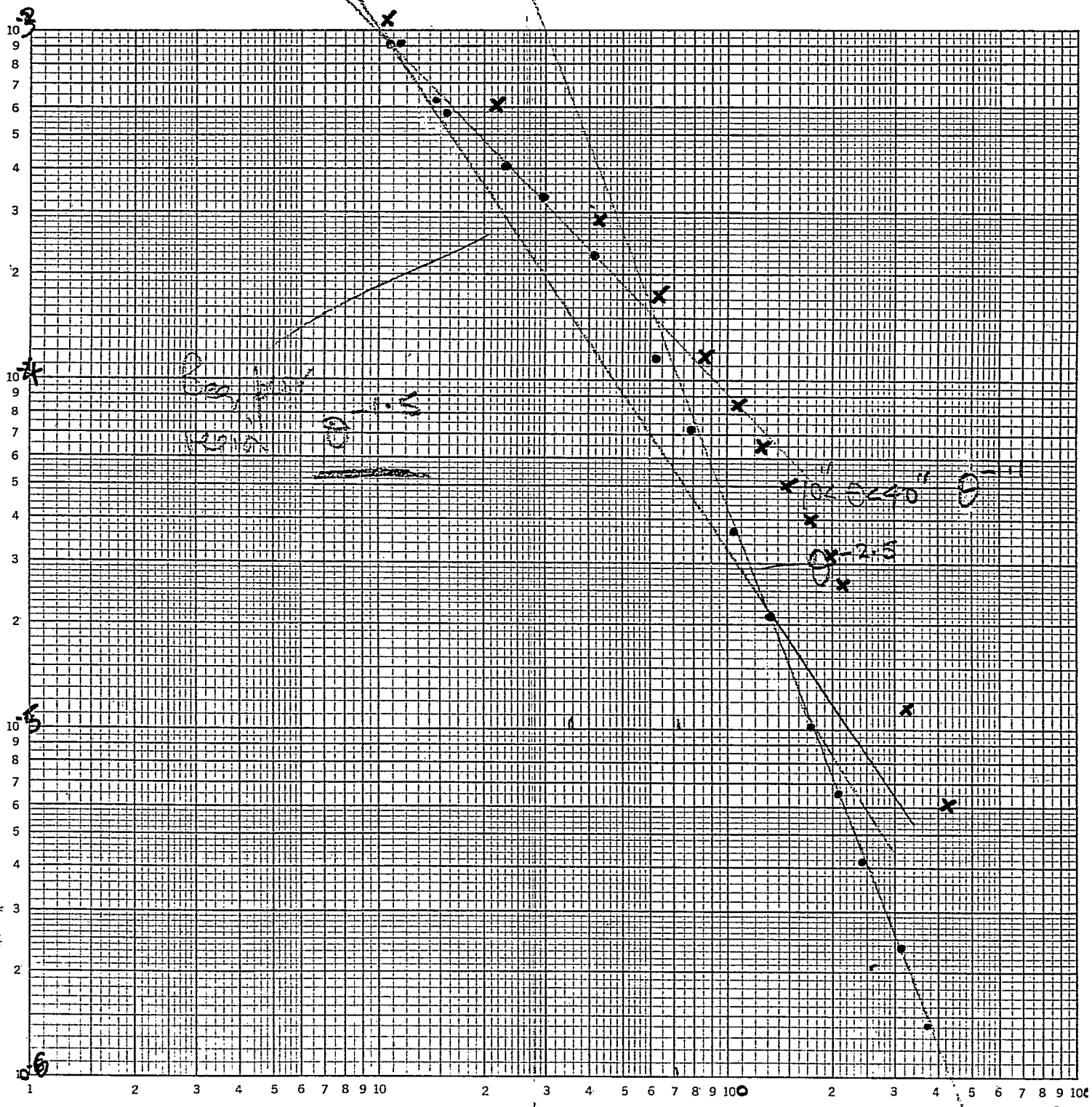




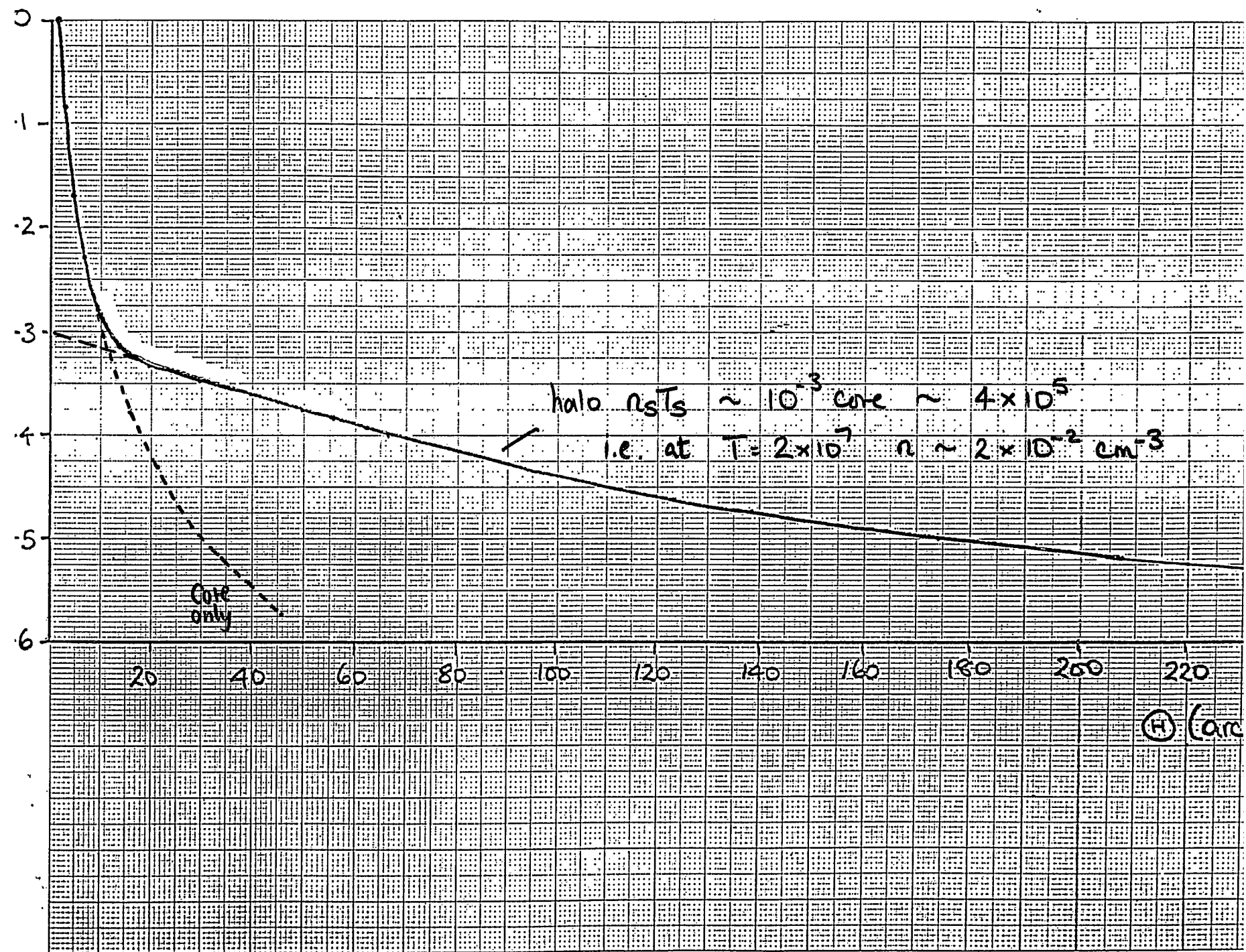
NGC 6251  
log-log  $\rho_e(z)$

46 7400

KE LOGARITHMIC 3 X 3 CYCLES  
KEUFFEL & ESSER CO. MADE IN U.S.A.







## Table 4

Minimum Mass and 0.5-4keV luminosity of media  
required to explain NGC6251 jet

Assumed Isothermal Temp.	$4 \times 10^7$ K	$2 \times 10^7$ K	$10^7$ K
$L_x$ (2.0 to 50 kpc), $\text{erg. s}^{-1}$	$1.3 \times 10^{42}$	$4.5 \times 10^{42}$	$1.1 \times 10^{43}$
$M$ (2.0 to 50 kpc), $M_\odot$	$3.8 \times 10^{10}$	$7.5 \times 10^{10}$	$1.5 \times 10^{11}$
$L_x$ (2.0 to 200 kpc), $\text{erg. s}^{-1}$	$1.5 \times 10^{42}$	$4.9 \times 10^{42}$	$1.2 \times 10^{43}$
$M$ (2.0 to 200 kpc), $M_\odot$	$1.2 \times 10^{11}$	$2.4 \times 10^{11}$	$4.7 \times 10^{11}$
$L_x$ (< 1.0 kpc), $\text{erg. s}^{-1}$	$4.7 \times 10^{43}$	$1.6 \times 10^{44}$	$3.8 \times 10^{44}$
$M$ (< 1.0 kpc), $M_\odot$	$7.6 \times 10^8$	$1.5 \times 10^9$	$3.0 \times 10^9$
$L_x$ (< 2.0 kpc)	$5.2 \times 10^{43}$	$1.7 \times 10^{44}$	$4.1 \times 10^{44}$
$M$ (< 2.0 kpc)	$1.2 \times 10^9$	$2.5 \times 10^9$	$5.0 \times 10^9$

Converted to pmc from Uur  
15 April 1983

## Outflow limit from lobe Dep $\alpha$ :

Willis, Wilson, Strom (1978)  $\rightarrow$   $n_e$  in lobe  $< 2 \times 10^{-5} \text{ cm}^{-3}$   
 $< 2 \times 10^7 \text{ m}^{-3}$

$$B_{eq} = 1.5 \times 10^{-6} \text{ gauss.}$$

$$\text{lobe radius} \sim 7'.5 = 450'' = 193 \text{ kpc} = 5.96 \times 10^{21} \text{ m}$$

$$\begin{aligned} \text{Mass in sphere of this radius} &= \frac{4}{3} \pi \times 20 \times 1.67 \times 10^{-27} \times (5.96 \times 10^{21})^3 \\ &= 2.96 \times 10^{40} \text{ kg} \\ &= 1.5 \times 10^{10} M_{\odot} \end{aligned}$$

## Entrainment Upper Limit

$$\frac{dm}{dt dl} = 2\pi R_j \Sigma_{IGM} C_{\Sigma_{IGM}}$$

10" from core

$$nT \sim 1.6 \times 10^5 \text{ cm}^{-3} \text{ K}$$

$$T \sim 3 \times 10^7$$

$$n \sim 5.33 \times 10^{-3} \text{ cm}^{-3}$$

$$p = 2.2 \times 10^{-12} \text{ J/m}^3$$

$$\rho = 8.9 \times 10^{-24} \text{ kg/m}^3$$

$$C_s = \sqrt{\frac{p}{\rho}} = 6.4 \times 10^5 \text{ m/s} = 640 \text{ km/s}$$

$$R_j = 0.75'' = 322 \text{ pc} = 9.93 \times 10^{18} \text{ m}$$

$$\text{Hence } \frac{dm}{dt dl} = 2 \times \pi \times 9.93 \times 10^{18} \times 8.9 \times 10^{-24} \times 6.4 \times 10^5 \text{ m/s}$$

$$= 3.55 \times 10^2 \text{ kg/m/sec}$$

$$= 1.09 \times 10^{22} \text{ kg/kpc/sec}$$

$$= 3.46 \times 10^{23} \text{ kg/kpc/yr}$$

$$= \underline{\underline{0.17 M_{\odot}/kpc/yr}}$$

i.e. the length scale for entraining its own flow rate must be  $\geq \frac{1.2 M_{\odot}/\text{yr}}{0.17 M_{\odot}/\text{kpc/yr}} \geq 7 \text{ kpc}$

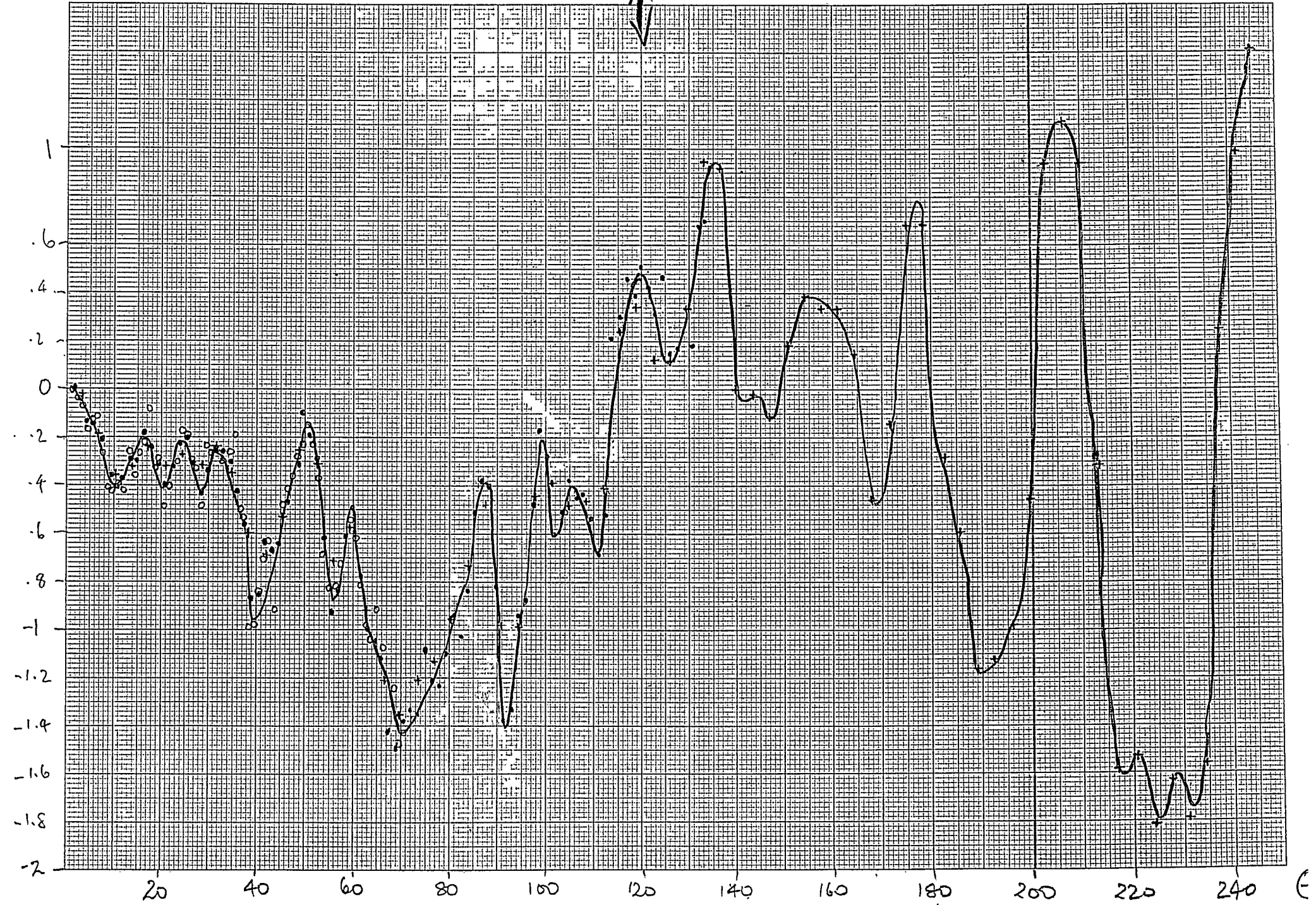
i.e. velocity could be halved by  $\sim 7 \text{ kpc}$  further down the jet  $\sim 16''$

i.e. by  $\theta \sim 26''$   $R_j = 1.84 \times R_{j0}$



0 < 150"

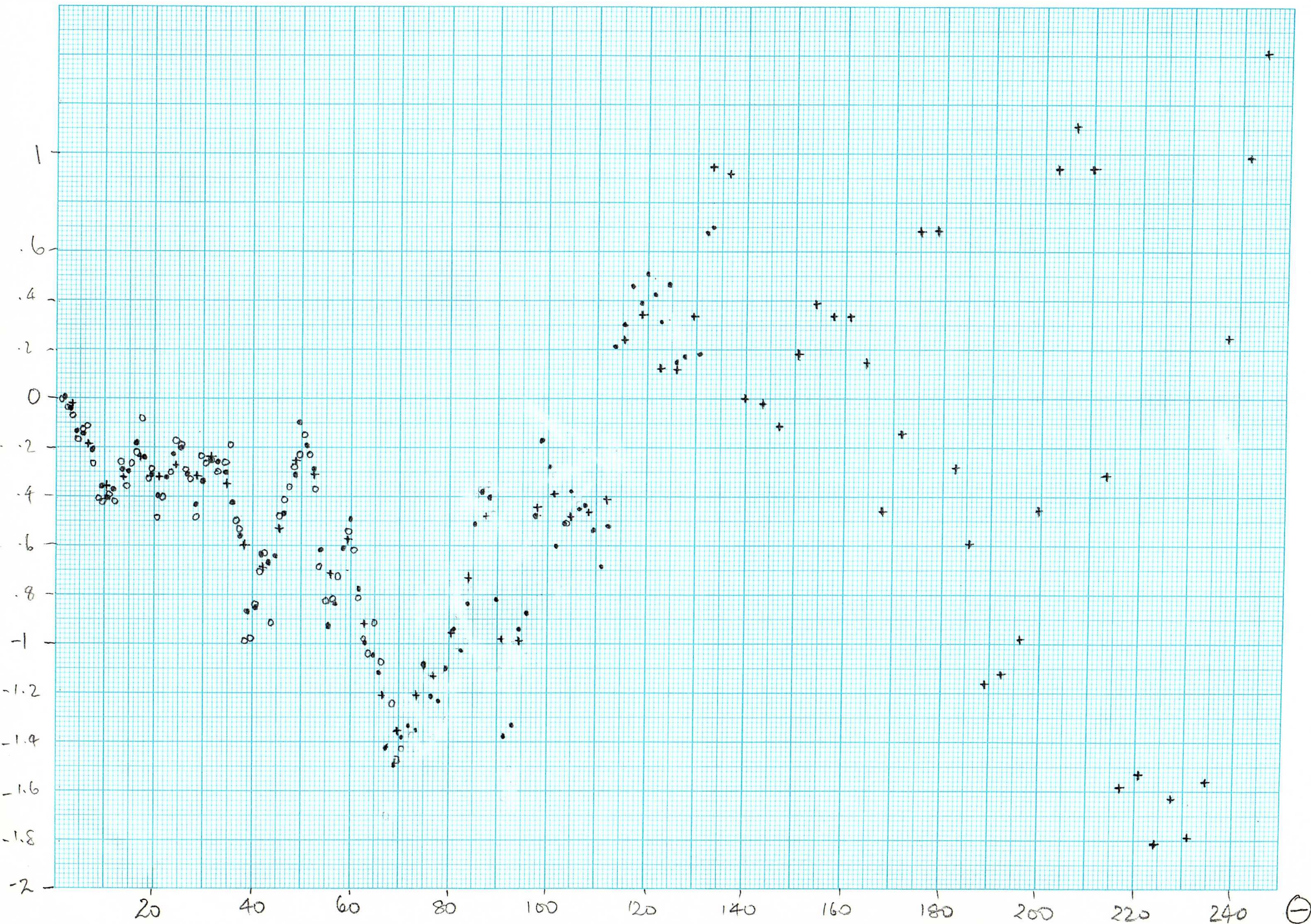
Δ





$\sigma < 150''$

$\Delta$



$\ominus$



Hanning Pressures

Power Sp. (512) (Inner Jer)

1"3 data  $\Delta(\theta)$  28" 17" 12".7 10".4 5".8  $\theta > 15".4$



$\Delta/\theta(\theta)$  25" 17".5 12".3 10".5 7".1 5".7  $\theta > 15".4$

(1024)



(27".8) (16".9) (9".0) (5".8) all  
(107" of data)

2".11 data  $\Delta(\theta)$  37".5 17".3 9".1 12".1?  $15" < \theta < 134"$



26".5 18"? 9".1 12".5  $15" < \theta < 100"$

$\Delta/\theta$  39".6 17".6 9".1 12".2 5".6  $15" < \theta < 134"$

54".9 24".9 18".3 12".4 9".1  $15" < \theta < 100"$

all

Conclude 9".1  
12".4 growing  
17".6?

Averaged  $\Delta/\theta$  2" cell

20" <  $\theta$  < 60"

20" <  $\theta$  < 80"

20" <  $\theta$  < 100"

20" <  $\theta$  < 120"

17".5  
11".8  
9".0  
17".8  
11".4  
9".5  
17".3  
11".6  
8".7  
17".1  
11".5  
8".7  
6".9

Conclude finally ] 9".0, 12".1, 17".5

Power Sp (S, 2) Outer Jer

			too short					
15" defa	$\Delta(\theta)$	140"	35".5	28".0			$\theta > 0$	
		143"		27".3			$\theta > 180"$	
	$\Delta/\theta(\theta)$	146"	35".5	26".3	58".6		$\theta > 0$	
		144"	34".7	27".4	56"		$\theta > 180"$	
4'.4 defa	$\Delta(\theta)$	(137")	31".2	23".3	17".1	12".6	9".4	$\theta > 0$
	$\Delta(\theta)$	(133")	31".3		17".2	12".6		$20 < \theta < 260$
	$\Delta/\theta(\theta)$	(151")	30".6	17".1	11".8	<del>58".6</del>		$\theta > 0$
	$\Delta/\theta(\theta)$	(140")	31".3	17".2	12".7	58".0		$20 < \theta < 260$



Conclude: 143" 57" ?  
 31".1  
 17".2  
 12".9

Over-all 143" 57"  
 31".1  
 17".5  
 12".1  
 9".0